



**REPORT NO. 3
CONTRACT NO. 3Z6248
(REPORT NO. 252, MRCE SERIES)
SECTIONS G4 AND G5, ADDISON ROUTE
PRELIMINARY SUBSURFACE INVESTIGATION**

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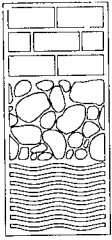
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May 16, 2000

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Re: Sections G4 and G5, Addison Route
Final Report
Preliminary Subsurface Investigation
MRCE File No. 8435A

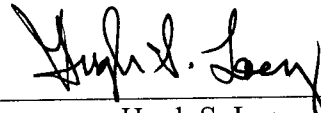
Dear Mr. Feng:

In accordance with our schedule, we submit herewith three copies of this final report for the subsurface investigation of Sections G4 and G5 of Addison Route, covering the planned Largo Town Center Station, and parking lots for the Summerfield Station and Largo Town Center Stations. Ten copies of this report have been sent to WMATA under separate cover. A draft of this report was submitted on June 16, 1998. No comments were received on the draft report. We believe that this completes all of the planned preliminary geotechnical investigations for this portion of the Addison Route.

Very truly yours,

MUESER RUTLEDGE CONSULTING ENGINEERS

By: _____


Hugh S. Lacy

DWC:HSL:bee9170\LTR-1

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1.0 INTRODUCTION

1.1 Authorization

Contract No. 3Z6248 between DeLeuw Cather & Company (DCCo) and Mueser Rutledge Consulting Engineers (MRCE) provides for subsurface investigations, laboratory testing and summary reports relating to certain sections of the Rapid Transit system. One portion of that report covers the making of 14 borings and six test pits as part of Phase II of preliminary subsurface investigation to provide geotechnical information in connection with the preparation of general plan drawings and preliminary design at 30% level. Three of the borings were drilled along the alignment of Largo Town Center station. The remaining 11 borings were drilled and six test pits were excavated at the planned locations of the Summerfield Station and Largo Town Center Station parking lots.

The following MRCE reports contain exploratory data obtained previously in Addison Route or information relevant to this section:

1. Final Report, Subsurface Investigation, Addison Route, Station 290 (G002) to 488 (G003), dated November, 1973 (MRWJ Series Report No. 95).
2. Supplementary Subsurface Investigation, Addison Route Section G003, dated November 22, 1974 (MRWJ Series Report No. 118).
3. Report on Pumping Test, Addison Route Section G003, dated July 7, 1975 (MRWJ Series Report No. 135).
4. Preliminary Subsurface Investigation, G-Route Addison Road to Largo Town Center, dated November 14, 1996 (MRCE Series Report No. 249).

1.2 Scope of Work

The scope of work comprises the subsurface investigation for the planned Largo Town Center Station, and parking lots for Summerfield and Largo Town Center Stations. The completed field work consists of a group of 14 borings and six test pits along the subway alignment and parking lots. A previous investigation along the subway alignment was performed in 1996 and the results published in MRCE Series Report No. 249. Borings Nos. MR-43U, MR-44 and MR-45U were drilled at the location of the planned Largo Town Center Station. Borings Nos. MR-18 through MR-

22 and Test Pits Nos. TP-1 and TP-2 were made in the Summerfield Station parking lot, and Borings Nos. MR-23 through MR-26, MR-46, MR-47 and Test Pits Nos. TP-3 through TP-6 were made in the Largo Town Center Station parking lot. Planned Boring No. MR-7 was deleted from the program because we were unable to obtain permission to access the site.

Boring operations commenced on March 30, 1998 following WMATA authorization to proceed, and the borings were completed on April 29, 1998. The test pits were excavated and backfilled on May 7, 1998. All borings were made by GeoServices Corporation under subcontract to Geotech Engineers Inc. and were inspected and logged by GeoServices. All test pits were made under subcontract to Geotech Engineers, Inc. and were inspected and logged by Geotech Engineers, Inc. An MRCE representative was present on a part time basis at the site during the borings and test pit operations to insure that the work was performed in accordance with Metro standards. The boreholes were made by conventional soil boring methods utilizing a tricone roller bit with the aid of casing and water to advance the hole. The test pits were excavated with a backhoe loader. Observation wells were installed in ten of the borings for continuing measurement of the groundwater levels. All borings with the exception of those containing observation wells were grouted at completion. All test pits were excavated and backfilled the same day. Corrosion tests on soil samples recovered from selected borings were performed by ARTECH Testing, LLC of Chantilly, VA under subcontract to Geotech Engineers, Inc. The results of these tests are included in the Appendix to this report.

All soil samples recovered from borings and test pits were transported to our New York City laboratory for examination, check of field classifications and performance of identification testing and engineering properties tests. Soil samples remaining after laboratory testing was completed were returned to Washington, DC and placed in the designated storage facility.

2.0 TEST BORING AND LABORATORY PROGRAM

2.1 Presentation of Boring Data

Locations of all 14 borings and six test pits are shown on Drawings Nos. GPG-SO-151, GPG-SO-290 and GPG-SO-310. Locations of the geological sections, as well as the general configuration of the Summerfield and Largo Town Center Stations and their corresponding parking lots are also shown on these drawings. Information from the completed borings of Largo Town Center Station as well as earlier borings is plotted in one geological section along the outbound track and is presented on Drawing No. GPG-SO-151. This drawing was originally presented in MRCE Series Report No. 249, dated November 9, 1996 and has been revised to incorporate data from current Borings Nos. MR-43U, MR-44 and MR-45U. Nine geological sections, Nos. A-A through J-J through the stations parking lots are presented on Drawings Nos. GPG-SO-320, GPG-SO-330, GPG-SO-340 and GPG-SO-350. All geological sections are drawn to scale distortion of one to four.

Soil data plotted on the geological sections include sample number designation and position, standard sample penetration resistance, Unified Soil Classification, water contents of fine grained soils, Atterberg Limits and shear strength in ksf. Also shown on the sections are the results of grain size tests on representative soil samples from the borings and test pits, giving the percentage by weight of particles passing the Nos. 200 and 40 sieves and of the gravel retained upon the No. 4 sieve. The legend explaining these test symbols is shown on the bottom of Drawing No. GPG-SO-320.

Final logs of the 14 borings and six test pits are presented on four Drawings Nos. GPG-SO-360 through GPG-SO-390. These logs are based on laboratory examinations of soil samples and identification testing, and they may differ in detailed interpretations from the driller's logs.

Coordinate locations and ground surface elevations of the borings and test pits are listed in Table No. 1. General Information Drawing No. F-1 presents notes and legend applicable to both the geological sections and boring log drawings. This drawing also summarizes the sequence of the principal subsurface strata with their general descriptions. The general strata descriptions of soils encountered in this design section are presented on the upper right corner of Drawing No. GPG-SO-320.

2.2 Laboratory Testing Program

Three- inch undisturbed samples were recovered by pushing thin Shelby tubes. Accepted samples were transported to our New York City laboratory for testing of engineering properties. Those tests comprised determination of shear strength by unconsolidated-undrained triaxial shear tests. In addition, Atterberg limit tests and grain size determinations were performed. The results of these tests are listed in Table No. 2, Summary of Laboratory Test Data. All split spoon samples were examined in the laboratory, classifications were checked and water content determined for clayey soils. Results of the plasticity tests are plotted on Plate No. 1. A total of 13 grain size determinations were performed on Tertiary soils of Strata Cs and Es and upper Cretaceous soils of Monmouth formation of Stratum Ms. Results are plotted on Plates Nos. 2 through 4. Eleven unconsolidated-undrained triaxial shear tests were performed on Tertiary soils of Stratum Es and Upper Cretaceous of Stratum Ms. Results of ten tests are presented on Plates Nos. 5 through 7. Three CBR tests were performed on materials of Aquia formation of Stratum Es. Results are presented on Plates Nos. 8 and 9.

2.3 Field Permeability Tests

Ten falling head permeability tests were performed in the borings with observation wells, and two falling head permeability tests were performed in the open borehole of Boring No. MR-22. Results are plotted in Table No. 3, which gives basic information on the circumstances of the test, stratum tested, and an average computed coefficient of permeability. The highest computed permeability

value is equal to 1.1×10^{-4} feet per minute in materials of Stratum Es. Because of muddy conditions in the borehole and in filter material of observation wells, the resulting values of estimated permeability tend to be lower than actual. They are not comparable in reliability to field pumping test results. Table No. 4 lists generalized coefficients of permeabilities of Pleistocene Terrace and Cretaceous soils based on full-scale, deep well pumping tests in earlier WMATA studies. Table No. 5 lists generalized coefficients of permeability of Tertiary and upper Cretaceous strata extrapolated from full-scale pumping tests on Pleistocene and Terrace soils based on a comparison of identification properties. The values on these two tables chiefly reflect the horizontal coefficients because of the flow conditions to the test wells. They are regarded as more realistic values than those given by the small scale tests in the individual boreholes.

2.4 Potential Corrosion Characteristics

Tests relating to potential corrosion characteristics included pH, resistivity, chlorides, sulfates, and total sulfur. Results of that testing are presented in the appendix to this report. Test on soil samples from Borings Nos. MR-18, MR-19, and MR-20 exhibited highly acidic pH values, and soil samples from Borings Nos. MR-43U and MR-44 exhibited total sulfur in excess of 500 ppm.

2.5 Groundwater Conditions

Water levels measured in observation wells installed in earlier borings and borings made for this investigation are indicated on the geological sections by a solid triangle symbol for the current borings and by an open triangle symbol for the earlier borings. An average water table position estimated from this group of readings is indicated by a dashed line on the geological sections. In general, the groundwater level is a subdued reflection of the ground surface. The groundwater level in the Summerfield Station parking lot rises from the east from about Elev. 185 in the vicinity of Summerfield Boulevard to about Elev. 205 near Boring No. MR-21. The groundwater level in the Largo Town Center Station parking lot rises to the north from about Elev. 130 in the vicinity of Boring No. MR-46 to about Elev. 165 near Arena Drive.

3.0 SUBSURFACE CONDITIONS

3.1 Subsoil Stratification

The subsoil stratification for the Addison Route comprising the entire subway alignment between stations 485+00 to 651+70.55 was summarized in MRCE Series Report No. 249, dated November 14, 1996. The principal materials encountered at the site of the planned Largo Town Center Station and parking lots for the Summerfield and Largo Town Center Stations comprise man-made fills, Tertiary Marine deposits of Calvert sands and clays of Strata Cs and Cc, Aquia sands and clays of Strata Es and Ec, upper Cretaceous Monmouth sands and clays of Strata Ms and Mc and Cretaceous clays and sands of Strata P1 and P2.

3.1.1 Stratum F-Fill Drawings Nos. SK-1, SK-2 and SK-3 show the existing ground surface at the site, in the years 1957, 1971, and 1993, respectively. These drawings indicate that very little fill has been added at the site, except in the northern portion of the Largo Town Center Station parking lot where up to about 23 feet of fill has been added. The fill is generally loose to medium compact sands and silts and medium to very stiff clays that are difficult to distinguish from the underlying soils from which they are derived, except where artificial materials are added. The thickness of fill generally varies between two and five feet except in the areas centered on Borings Nos. MR-43U and MR-46 where the fill ranges between about 18 and 23 feet.

3.1.2 Stratum Cc (Calvert) Plastic Clay, Silty and Sandy Clay or Clayey Silt This is a medium to stiff dark gray, green, brown, and yellow orange plastic clay, silty and sandy clay or clayey silt, trace fine sand, gravel. The Calvert is a Tertiary marine deposit laid down under changing depositional conditions. This clay was encountered only in Boring No. MR-14, located west of the Summerfield Station. The Calvert clays are substantially overconsolidated to stresses of 7 to 12 tsf and shear strength increases with depth from about 1.5 to 2.5 ksf.

3.1.3 Stratum Cs (Calvert) Fine Sand, Trace to some Silty Clay and Silty or Clayey Fine Sand Stratum Cs consists of loose to medium compact dark gray, olive gray, green brown and yellow orange fine sand, trace to some silt, clay and silty or clayey fine sand, trace gravel. This stratum was encountered in Borings Nos. MR-14, MR-15U and MR-21 overlying the Es sands. Standard penetration test resistance is in the range of 5 to 16 blows per foot. The low blow count is apparently due to sampling techniques and does not represent a variation in the density of the stratum. Although the stratum is rated as loose to medium compact based on the standard penetration resistance recorded in the borings, the actual consistency can be classified as medium compact.

3.1.4 Stratum Ec (Aquia) Plastic to Silty and Sandy Clay or Clayey Silt This stratum consists of medium to stiff gray, green, olive gray plastic clay to silty and sandy clay or clayey silt, trace lignite with occasional slightly organic fine sandy and silty clay layers, trace shells. This is the oldest of the Tertiary marine sediments and it was encountered in Borings Nos. MR-16U, MR-19 and MR-25 at the Summerfield Station structure and parking lot, and in Boring No. MR-48U located near the east end of the Largo Town Center Station platform. The clay is preconsolidated in the range of 7 to 8 tsf, and shear strengths increase with depth from about 2 to 3.5 ksf.

3.1.5 Stratum Es (Aquia) Silty and Clayey Fine Sand This stratum consists of loose to medium compact green, olive gray silty and clayey fine sand, trace shells, mica with occasional slightly organic silty and clayey fine sand layers. This stratum was encountered throughout Summerfield and Largo Town Center Stations and their parking lots, overlying the Monmouth formation of Stratum Ms. Standard penetration resistance apparently is low due to sampling techniques, and does not represent a true variation in consistency. Although the stratum is rated as loose to medium compact based on the standard penetration resistance recorded in the borings, the actual consistency can be classified as medium compact based on the results of strength tests on undisturbed samples of Es sands, conducted for earlier WMATA investigations.

3.1.6 Stratum Mc (Monmouth) Slightly Organic Fine Sandy Silt and Clayey Silt This material comprises loose to very compact dark green slightly organic micaceous fine sandy silt, and very stiff to hard clayey silt, trace shells, occasionally cemented. This stratum belongs to the upper Cretaceous deposits and it was found in Boring No. MR-16U at the Summerfield Station, and in Borings Nos. MR-43U, MR-44 and MR-45U located at and west of the Largo Town Center Station. This formation is heavily preconsolidated in excess of 10 tsf. Shear strengths generally range between 3 and 3.5 ksf based on tests performed earlier for other WMATA design sections.

3.1.7 Stratum Ms (Monmouth) Slightly Organic Micaceous Silt, Fine Sand and Clayey Fine Sand This stratum consists of loose to very compact dark green slightly organic micaceous silty fine sand, trace clay and clayey fine sand, trace to some shells, occasionally cemented, and with cemented sand layers. This sandy material is present east of Station 492 and it is continuous until the end of the alignment at Station 632 and overlies the Cretaceous deposits. Standard penetration resistance is generally between 10 and 30 blows per foot, and in a few instances exceeds 100 blows per foot, reflecting the presence of cemented shell and cemented sand pockets and lenses.

Although the Monmouth formation of Strata Mc and Ms is classified as loose to very compact based on the standard penetration resistance, the actual consistency can be classified as medium to very compact, based on results of strength tests and its high degree of preconsolidation and significant cementation.

3.1.8 Stratum P1 (Cretaceous) Plastic Clay Primarily stiff to hard red-brown and gray or light gray plastic clay, silty clay, CH or CL by the Unified Soil Classification System. This stratum is present generally below about Elev. 110 underlying the Monmouth formation. It was found in deep Borings Nos. MR-40 through MR-45. The distinctive characteristics of these mottled red-brown and gray clays is that they are frequently fissured or slickensided. Shear strengths of intact samples tested generally ranged between 3 and 7 ksf. This stratum is not continuous throughout the alignment and it is frequently interlayered with materials of Strata P1 (CL) and P2.

3.1.9 Stratum P1 (CL) (Cretaceous) Sandy Clay Stiff to hard gray silty or sandy clay, with some fine sand layers, trace to some cemented sand and lignite fragments. Shear strengths have a narrower range than the plastic clays of Stratum P1 since slickensides are not particularly numerous. This stratum is frequently interlayered with plastic clays of Stratum P1, and sands of Stratum P2.

3.1.10 Stratum P2 (Cretaceous) Silty or Clayey Sand The P2 stratum consists of compact to very compact, light gray, brown or tan fine to medium sand, some clay, silt or clayey fine to medium sand, trace cemented sand layers, gravel, lignite. It is interlayered with materials of Strata P1 (CL) and P2 (SP-SM).

4.0 SUMMARY OF DESIGN AND CONSTRUCTION PROBLEMS

4.1 Largo Town Center Station

Location of the Largo Town Center Station is shown in geological section on Drawing No. GPG-SO-151. Subsurface conditions consist of a layer of fill ranging in thickness between about five and 18 feet thick overlying in order of depth, Aquia sands and clays of Strata Es and Ec, Monmouth sands and clays of strata Ms and Mc and Cretaceous clays and sands of Strata P1, P1(CL), and P2. The groundwater level is a subdued reflection of the ground surface, ranging between about Elev. 127 and Elev. 158. Because of the presence of a relatively thick layer of loose to medium fill, spread bearing foundations on new embankment for support of the station structure are not indicated; therefore, pile support of the station appears necessary.

Piles of up to 70 ton capacity could consist of steel H-piles, closed-end pipe or precast concrete piles. We estimate 70 ton pile penetrations below the top of the Monmouth formation of Stratum Ms of about 15 to 20 feet for pipe piles and precast concrete piles and about five to ten feet deeper for H-piles. Fills of up to 13 to 14 feet will be required at the western end of the station. Pile design should include an analysis of the potential downdrag created by these fills.

4.2 Summerfield Station Parking Lot

General configuration of the planned parking lot and borings and test pits in the area are depicted on the general location plan on Drawing No. GPG-SO-290. Geological Sections Nos. A-A and B-B are presented on Drawing No. GPG-SO-320, and Geological Section C-C is shown on Drawing No. GPG-SO-330. Subsurface conditions consist of a relatively thin layer of fill averaging five feet thick overlying in order of depth, Calvert sands of Strata Cs, Aquia sands and clays of Strata Es and Ec followed by Monmouth sands and clays of Strata Ms and Mc. The groundwater level is about one to five feet below existing ground surface. Subgrade will be primarily on a new fill and in certain localized areas will be on a shallow cut. Fill heights are generally less than 6 feet, with a maximum of 10 feet in the northeastern portion of the lot.

In cut areas, the surface of the existing materials should be thoroughly proofrolled before placing the pavement base. In fill areas, the unsuitable materials should be removed from the existing ground surface, and the areas proofrolled before placing the controlled fill. The new fill should consist of "materials for embankment fill" meeting WMATA specifications, Section 204, Article 2.1A. For the sake of uniformity, a CBR of 7 can be used for the design of the flexible pavement in cut and fill areas even though a CBR equal to ten was obtained in the laboratory test on Aquia sands of Stratum Es recovered in Test Pit No. TP-2.

4.3 Largo Town Center Station Parking Lot

General configuration of the planned parking lot and borings and test pits in the area are shown on the general location plans on Drawings Nos. GPG-SO-300 and GPG-SO-310. A group of six geological sections Nos. D-D through J-J depict the subsurface conditions through the parking lot. Geological Section D-D is presented on the bottom panel of Drawing No. GPG-SO-330. Geological Sections Nos. E-E and F-F are depicted on Drawing No. GPG-SO-340 and Geological Sections Nos.

G-G through J-J on Drawing No. GPG-SO-350. Subsurface conditions consist of a layer fill ranging in thickness roughly between two feet and 23 feet as disclosed by Boring No. MR-46. The fill thickness appears to increase from east to west. The fill overlies in order of depth Aquia sands and clays of Strata Es and Ec, Monmouth sands and clays of Strata Ms and Mc followed by Cretaceous clays and sands of Strata P1, P1(CL) and P2. The groundwater level is in general between two and fifteen feet below the ground surface. As shown on the plan on Drawing No. GPG-SO-300, a stream is present the northern limit of the western parking lot which would have to be piped prior to the construction of the parking lot.

Subgrade of the lot will be primarily on a new controlled fill of up to 12 feet in thickness, with exception of localized areas that will be in cut. Proposed grades in the northeast parking lot are not well defined at this time, but fills in this area could reach 20 feet. This will require a retaining wall around three sides of the parking lot. In fill areas, the unsuitable materials and old pavement should be removed from the existing ground surface, including the material from an undercut of about five feet of loose fill in the general area of Boring No. MR-46, and the old stream, and then the area proofrolled before placing the controlled fill. The new fill should consist of "materials for embankment fill" meeting WMATA Specifications, Section 204, Article 2.1.A. A CBR of 7 for the controlled fill can be used for the design of the flexible pavement in cut and fill areas. CBR tests were performed in the laboratory on representative samples of Aquia sands of Stratum Es recovered from Test Pit Nos. 3 and 6 at about two feet below the existing ground surface. The results of the tests disclosed a CBR equal to 10 and 14 . Because most of the parking lot area will be on a new controlled fill, the use of CBR of 7 for the entire lot is justified.

TABLE NO. 1, SURVEY DATA FOR BORINGS (SECTIONS G4 AND G5 - ADDISON ROUTE)

BORING NUMBER	HORIZONTAL CONTROL COORDINATES:		VERTICAL CONTROL: GROUND SURFACE ELEVATION (FT)	STATUS OF OBSERVATION WELLS		
	NORTH	EAST		INSTALLED	TYPE	PRESENT CONDITION
MR-7	DELETED					
MR-18	446,505	1,349,554	206.8	04-23-98	1-1/2"	F
MR-19	446,694	1,349,954	197.9	04-27-98	1-1/2"	F
MR-20	446,107	1,349,742	208.5	04-24-98	1-1/2"	F
MR-21	446,076	1,350,060	210.4	04-29-98	1-1/2"	F
MR-22	446,505	1,350,228	195.0	04-28-98	1-1/2"	F
MR-23	449,018	1,356,475	152.5			
MR-24	449,207	1,356,769	155.0	04-06-98	1-1/2"	F
MR-25	450,098	1,357,155	149.4	04-22-98	1-1/2"	F
MR-26	450,518	1,356,911	173.1			
MR-43U	449,735	1,356,380	145.4	04-21-98	1-1/2"	F
MR-44	449,946	1,356,499	149.8			
MR-45U	450,179	1,356,606	158.4			
MR-46	449,326	1,355,858	142.4	04-06-98	1-1/2"	F
MR-47	448,841	1,356,125	147.4	04-03-98	1-1/2"	F
TP-1	446,463	1,349,777	204.8			
TP-2	446,294	1,349,888	203.0			
TP-3	449,326	1,356,507	146.5			
TP-4	449,737	1,356,898	145.4			

TABLE NO. 1, SURVEY DATA FOR BORINGS (SECTIONS G4 AND G5 - ADDISON ROUTE - CONT'D)

BORING NUMBER	HORIZONTAL CONTROL COORDINATES:		VERTICAL CONTROL: GROUND SURFACE ELEVATION (FT)	STATUS OF OBSERVATION WELLS		
	NORTH	EAST		INSTALLED	TYPE	PRESENT CONDITION
TP-5	449,980	1,356,671	152.5			
TP-6	450,361	1,357,000	162.1			

LEGEND

F - Indicates observation well functioning in 1998.

TABLE NO. 2

SUMMARY OF LABORATORY TEST DATA

SAMPLE IDENTIFICATION				CLASSIFICATION PROPERTIES									PHYSICAL PROPERTIES														
													STRENGTH						CONSOLIDATION								
BORING NUMBER	SAMPLE NUMBER	DEPTH FT.	STRATUM DESIGNATION	NATURAL WATER CONTENT % (W) AVERAGE OF ENTIRE SAMPLE	LIQUID LIMIT (W _L)	PLASTICITY INDEX (I _p)	NATURAL WATER CONTENT OF LIMIT SAMPLE, W _n , %	SPECIFIC GRAVITY OF SOLIDS (G _s)	DRY DENSITY, PCF	UNIFIED SOIL CLASSIFICATION SYSTEM			UNCONFINED COMPRESSION			TRIAXIAL COMPRESSION						NATURAL WATER CONTENT, W _n , %	EXISTING OVERBURDEN STRESS P ₀ , TSF	ESTIMATED PRECONSOLIDATION STRESS P _c , TSF	COMPRESSION INDEX, C _c	SWELLING INDEX, C _s	VOID RATIO AT START OF SWELL, e _r
										SOIL TYPE	% SAND (<# 4 >#200 SIEVE)	% FINES (<#200 SIEVE)	COMPRESSIVE STRENGTH TSF	WATER CONTENT AT END OF TEST, %	STRAIN AT FAILURE, %	TYPE OF TEST	DEVIATOR STRESS (σ ₁ -σ ₃), TSF	CONFINING PRESSURE (σ ₃), TSF	NATURAL WATER CONTENT, W _n , %	WATER CONTENT AT END OF TEST, W _t , %							
MR-43U	9U	17	F ES	33 34					92	SM-SC SM-SC							Q Q	0.79 1.61	0.5 0.99	34 34	34 34						
	11U	21	MS	27					98	SM-SC SM-SC SM-SC	63	37					Q Q Q	2.22 3.52 4.41	0.5 1.00 2.00	27 25 27	27 26 27						
MR-45U	6U	11	ES	37					83	SM SM SM	69	31					Q Q Q	1.48 1.03 1.94	0.50 1.00 2.00	38 36 36	38 37 37						
	10U	18.9	MS	25				2.72		SP-SM SP-SM	90	10					Q Q	2.66 3.02	0.50 1.00	25 24	26 25						
	13U	26.8	MS	27						SM-SC							Q	3.70	2.00	26	27						

- ALL TESTS SUMMARIZED ABOVE WERE PERFORMED IN THE SOILS LABORATORY OF MUESER RUTLEDGE CONSULTING ENGINEERS.
- THE SAMPLE DEPTH LISTED ABOVE IS THE AVERAGE DEPTH OF THE SAMPLE RECOVERED.
- FOR GROUND SURFACE ELEVATIONS AT THE BORINGS SEE TABLE NO. 1. FOR GENERALIZED STRATA DESCRIPTIONS SEE DRAWING NO. F-1.
- "NATURAL WATER CONTENT OF THE ENTIRE SAMPLE" IS A WEIGHTED AVERAGE OF ALL MATERIAL TYPES RECOVERED.
- THE TRIAXIAL COMPRESSION TESTS PERFORMED WERE:
 - Q - QUICK TESTS (UU - UNCONSOLIDATED UNDRAINED TESTS)
 - Qc - CONSOLIDATED QUICK TESTS (CU - CONSOLIDATED UNDRAINED TESTS)
- STRENGTH TESTS WERE PERFORMED ON PISTON TYPE SAMPLES (U) APPROXIMATELY 2.9 INCHES IN DIAMETER AND ON SHELBY TYPE SAMPLES (S) APPROXIMATELY 1.8 INCHES IN DIAMETER. THE RATIO OF HEIGHT TO DIAMETER OF ALL STRENGTH TEST SPECIMENS WAS APPROXIMATELY 2.0.
- THE TRIAXIAL COMPRESSION TESTS WERE PERFORMED AT A RATE OF STRAIN OF APPROXIMATELY 1 PER CENT PER MINUTE.
- THE DIRECT SHEAR TESTS WERE PERFORMED AT A CONSTANT RATE OF STRAIN EQUAL TO A HORIZONTAL DISPLACEMENT OF 0.02 INCHES PER HOUR. THE SPECIMENS WERE OF APPROXIMATELY 1/2 INCH THICKNESS.
- COMPRESSION INDEX C_c - STRAIGHT LINE PORTION OF THE VIRGIN CURVE OF CONSOLIDATION TEST: $e = e_0 - C_c \log P/P_0$
- SWELLING INDEX C_s - STRAIGHT LINE PORTION OF THE REBOUND CURVE OF CONSOLIDATION TEST: $e = e_0 - C_s \log P/P_0$

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**TABLE NO. 3, SUMMARY OF RISING AND FALLING HEAD PERMEABILITY TESTS IN BOREHOLES AND OBSERVATION WELLS
(SECTION G - ADDISON ROUTE)**

BORING NO.	MR-18 (OBSERVATION WELL)	MR-19 (OBSERVATION WELL)	MR-20 (OBSERVATION WELL)	MR-21 (OBSERVATION WELL)	MR-22 (OBSERVATION WELL)	MR-22 (BOREHOLE)
TYPE OF TEST	FALLING HEAD	FALLING HEAD	FALLING HEAD	FALLING HEAD	FALLING HEAD	FALLING HEAD TEST NO. 1
ELEVATION OF TOP AND BOTTOM OF OPENING TESTED	+ 183.8 + 166.8	+ 184.9 + 167.9	+ 195.5 + 178.5	+ 197.4 + 180.4	+ 182.0 + 165.0	+ 190.3 + 179.5
LENGTH OF OPENING IN FEET	17.0	17.0	17.0	17.0	17.0	10.8
AVERAGE COMPUTED PERMEABILITY, FEET/MINUTE	2.7×10^{-5}	2.3×10^{-5}	1.0×10^{-5}	3.0×10^{-5}	8.6×10^{-5}	1.1×10^{-4}
STRATUM TESTED	Ms	Es & Ms	Es & Ms	Es & Ms	Es & Ms	Es
BORING NO.	MR-22 (BOREHOLE)	MR-24 (OBSERVATION WELL)	MR-25 (OBSERVATION WELL)	MR-43U (OBSERVATION WELL)	MR-46 (OBSERVATION WELL)	MR-47 (OBSERVATION WELL)
TYPE OF TEST	FALLING HEAD TEST NO. 2	FALLING HEAD	FALLING HEAD	FALLING HEAD	FALLING HEAD	FALLING HEAD
ELEVATION OF TOP AND BOTTOM OF OPENING TESTED	+ 176.5 + 174.5	+ 142.0 + 125.0	+ 136.4 + 119.4	+ 82.9 + 65.4	+ 129.4 + 112.4	+ 132.4 + 117.4
LENGTH OF OPENING IN FEET	2.0	17.0	17.0	17.5	17.0	15.0
AVERAGE COMPUTED PERMEABILITY, FEET/MINUTE	2.5×10^{-5}	1.2×10^{-5}	5.6×10^{-5}	6.9×10^{-7}	4.4×10^{-6}	2.0×10^{-6}
STRATUM TESTED	Ms	Ms	Ms	P1, P1,CL & P2	F, Es & Ms	Es & Ms

TABLE NO. 4

REPRESENTATIVE PERMEABILITY VALUES

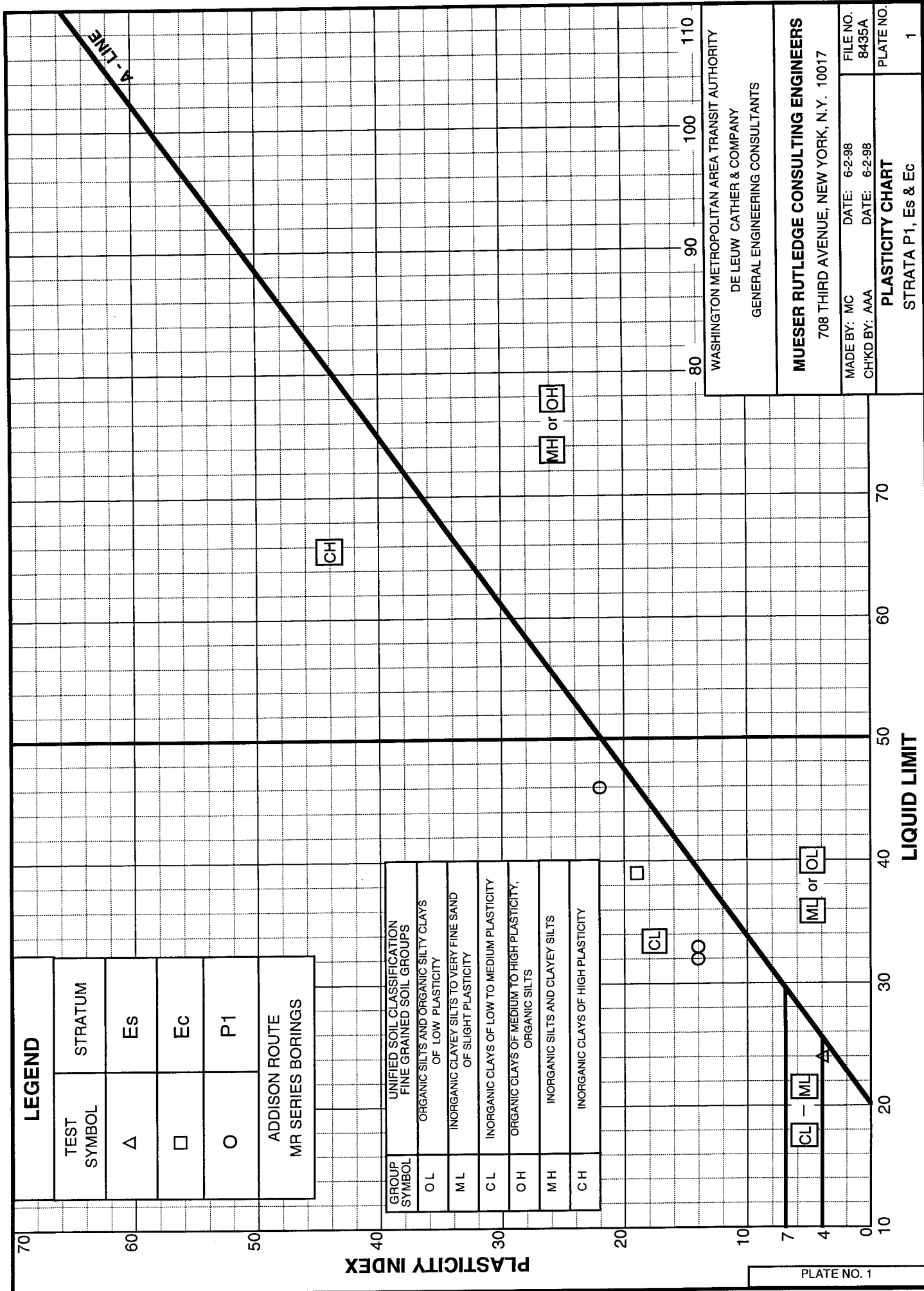
STRATUM	SOIL TYPE	COEFFICIENT OF PERMEABILITY K, (FT/MIN)
A1	Organic Clay	10^{-5} to 10^{-6}
A2	Silty Sand	10^{-3} to 10^{-4}
T0	Organic Clay	10^{-5} to 10^{-6}
T1	Silty Clay	10^{-5} to 10^{-6}
T2	Silty Sand	10^{-3} to 10^{-5}
T3	Gravelly Sand	5×10^{-2} to 10^{-3}
T4	Silty Sand	10^{-3} to 10^{-4}
T5	Gravelly Sand	5×10^{-2} to 10^{-3}
P1	Clay	10^{-7} Typical
P2	Clayey Sand	10^{-3} to 10^{-5}
P3	Sandy Clay	10^{-4} to 10^{-6}

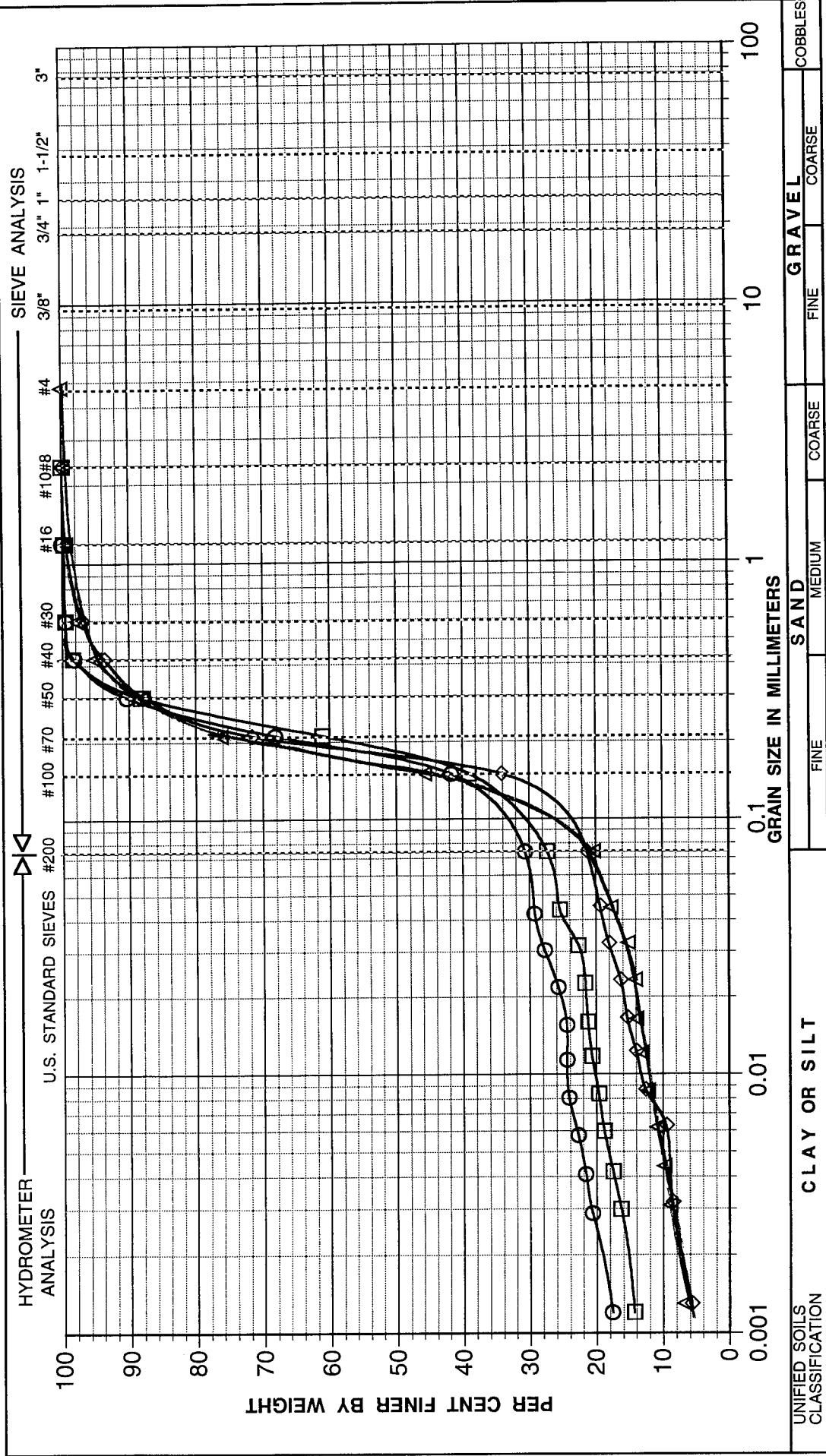
NOTE:

Range of permeabilities shown in this table is a general summary based on full scale pumping tests in earlier WMATA studies. The permeability values determined from small samples of the various strata or from borehole permeability tests frequently fall outside of the range noted.

TABLE NO. 5
REPRESENTATIVE PERMEABILITY VALUES

STRATUM	SOIL TYPE	COEFFICIENT OF PERMEABILITY K, (FT/MIN)
Q2	Fine to coarse sand, some medium to coarse gravel	5×10^{-2} to 10^{-3}
Cc	Plastic clay, silty and sandy clay or clayey silt	10^{-6} to 10^{-7}
Cs	Fine sand, trace to some silt, clay and clayey fine sand	10^{-3} to 10^{-5}
Ec	Plastic clay to silty and sandy clay or clayey silt	10^{-6} to 10^{-7}
Es	Silty and clayey fine sand	10^{-3} to 10^{-5}
Mc	Slightly organic fine sandy silt and clayey silt	10^{-5} to 10^{-6}
Ms	Slightly organic micaceous silty or clayey fine sand	10^{-3} to 10^{-5}





			DESCRIPTION OF SAMPLE					
					STRATUM Es			

HYDROMETER ANALYSIS



U.S. STANDARD SIEVES

SIEVE ANALYSIS

#200 #100 #70 #50 #40 #30 #16 #10 #8 #4

3/8" 1/2" 1" 3"

PER CENT FINER BY WEIGHT

0 10 20 30 40 50 60 70 80 90 100

0.001 0.01 0.1 1 10 100

GRAVEL

SAND

CLAY OR SILT

COBBLES

COARSE FINE COARSE FINE

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MADE BY: MC DATE: 6-4-98
CH'KD BY: AAA DATE: 6-4-98

FILE NO. 8435A
PLATE NO. 3

STRATUM (Es)

GRADATION CURVES

STRATUM (Es)

DESCRIPTION OF SAMPLE

SYMBOL BORING SAMPLE

MR-24 TP-2 TP-3 TP-6

4D 1B 1B 1B

PLATE NO. 3

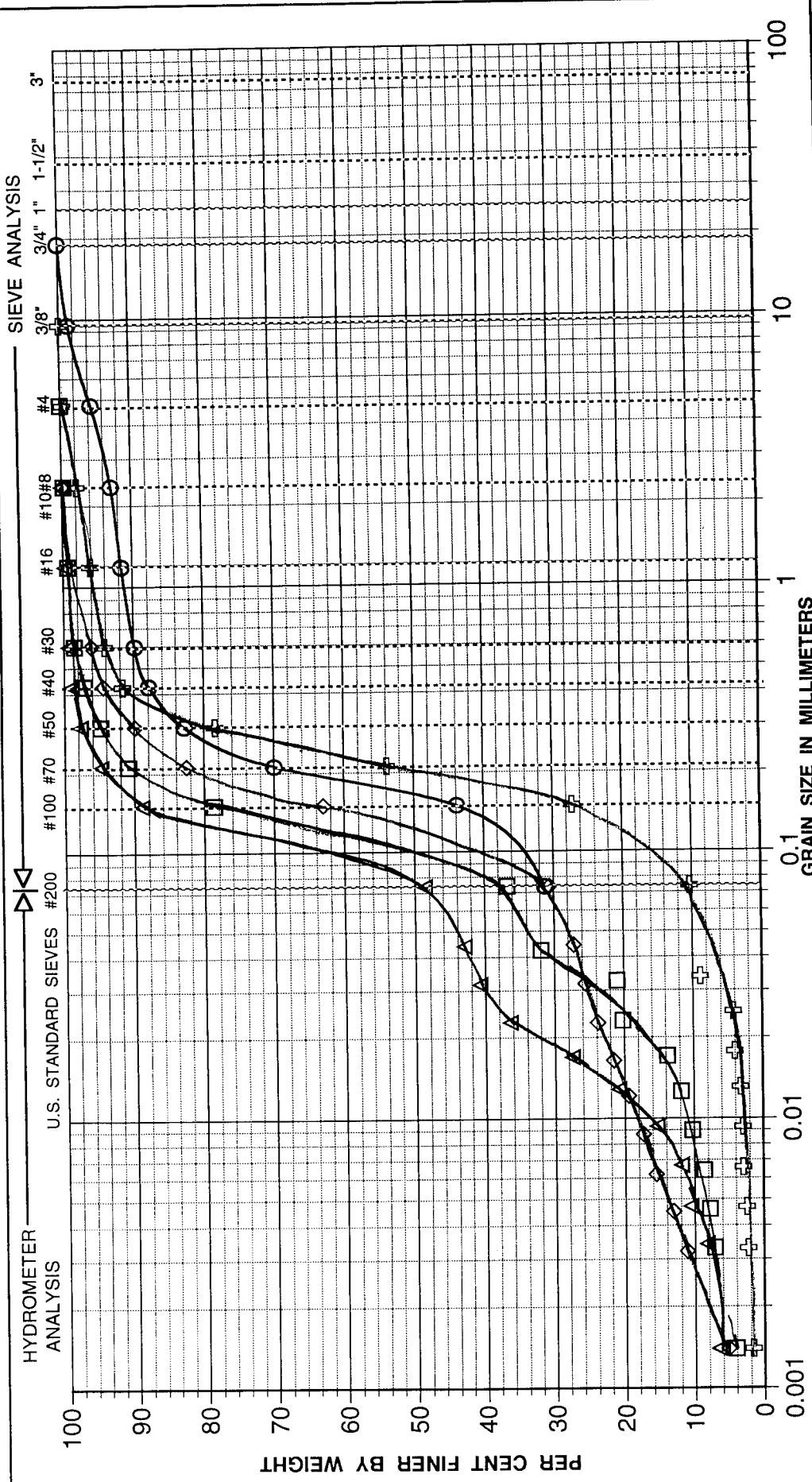
STRATUM (Es)

GRADATION CURVES

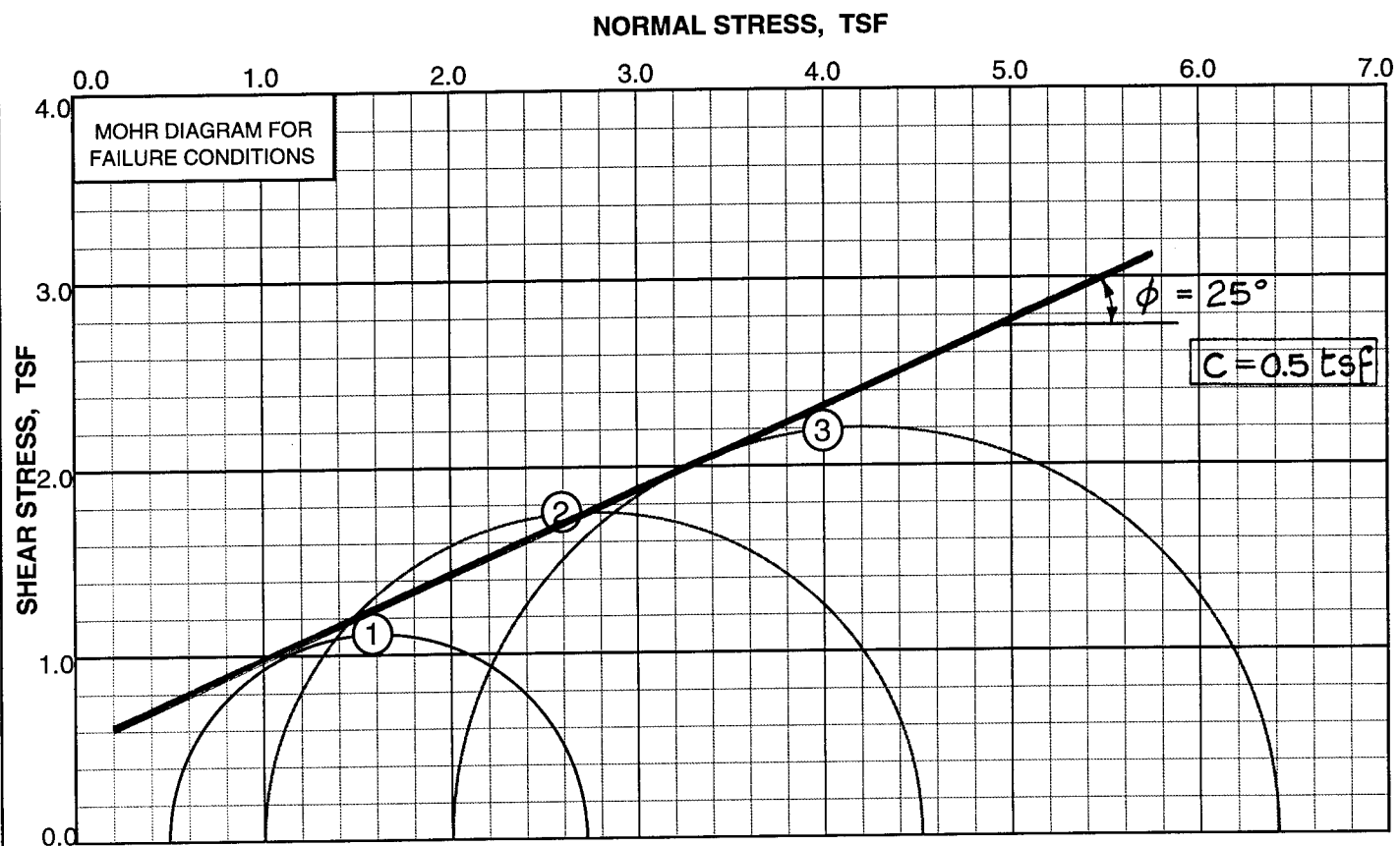
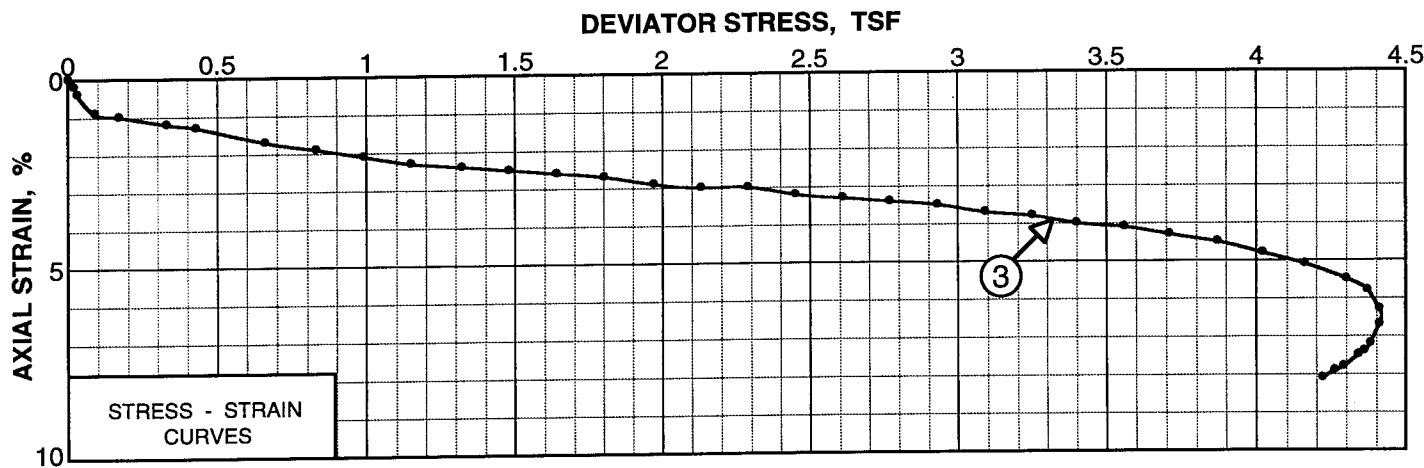
STRATUM (Es)

STRATUM (Es)

STRATUM (Es)



UNIFIED SOILS CLASSIFICATION				CLAY OR SILT				SAND				GRAVEL				COBBLES			
SYMBOL		BORING		SAMPLE		STRATA		DESCRIPTION OF SAMPLE				FINE		COARSE		FILE NO.			
○		MR-21		2D		Cs		STRATA (Cs), (Es) & (Ms)				MADE BY: MC		DATE: 5-27-98		FILE NO. 8435A			
□		MR-43U		11U		Ms						CH'KD BY: AAA		DATE: 5-27-98		PLATE NO. 4			
△		MR-44		10D		Ms						GRADATION CURVES							
◇		MR-45U		6U		Es													
⊕		MR-45U		10U		Ms													
WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY DeLEUW, CATHER AND COMPANY GENERAL ENGINEERING CONSULTANTS																MUESER RUTLEDGE CONSULTING ENGINEERS 708 THIRD AVENUE, NEW YORK, N.Y. 10017			
PLATE NO. 4																			



DESCRIPTION OF MATERIAL TESTED

DARK GRAY SLIGHTLY ORGANIC MICACEOUS SILTY FINE SAND, TRACE CLAY, SHELLS, MEDIUM TO COARSE SAND, SHELL LAYERS, GRAVEL STRATUM (MS)

SYMBOLS FOR TEST TYPES

Q - UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST

KEY	BORING NO.	SAMPLE NO.	SOIL TYPE	TEST TYPE	LATERAL PRESSURE TSF	WATER CONTENT-%		DEGREE OF SATURATION-%		DEVIATOR STRESS TSF	AXIAL STRAIN %
						INITIAL	FINAL	INITIAL	FINAL		
1	MR-43U	11U	SM-SC	Q	0.50	27	27			2.22	8
2	MR-43U	11U	SM-SC	Q	1.0	25	26			3.52	5
3	MR-43U	11U	SM-SC	Q	2.0	27	27			4.41	6

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DATE: 6-1-98

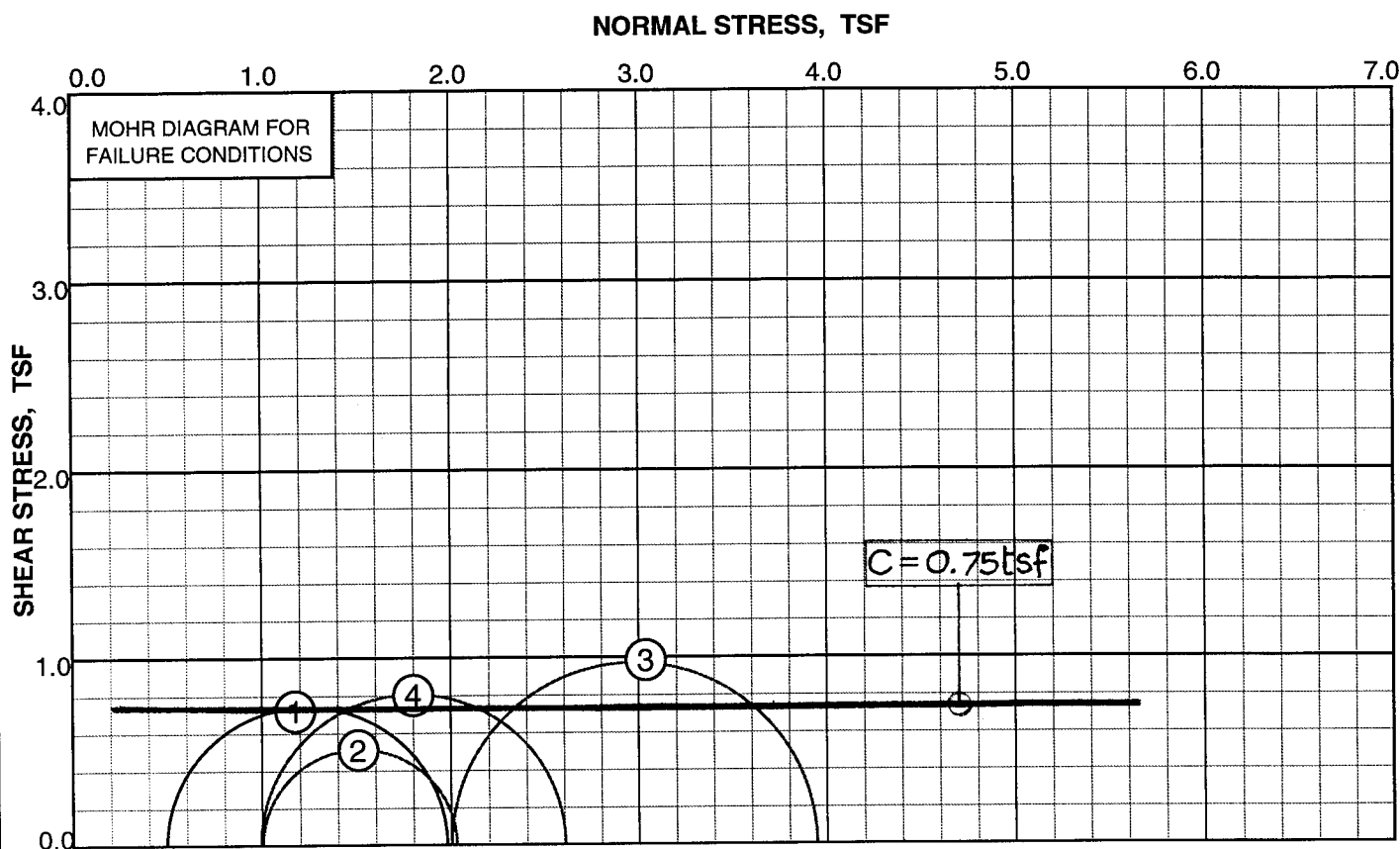
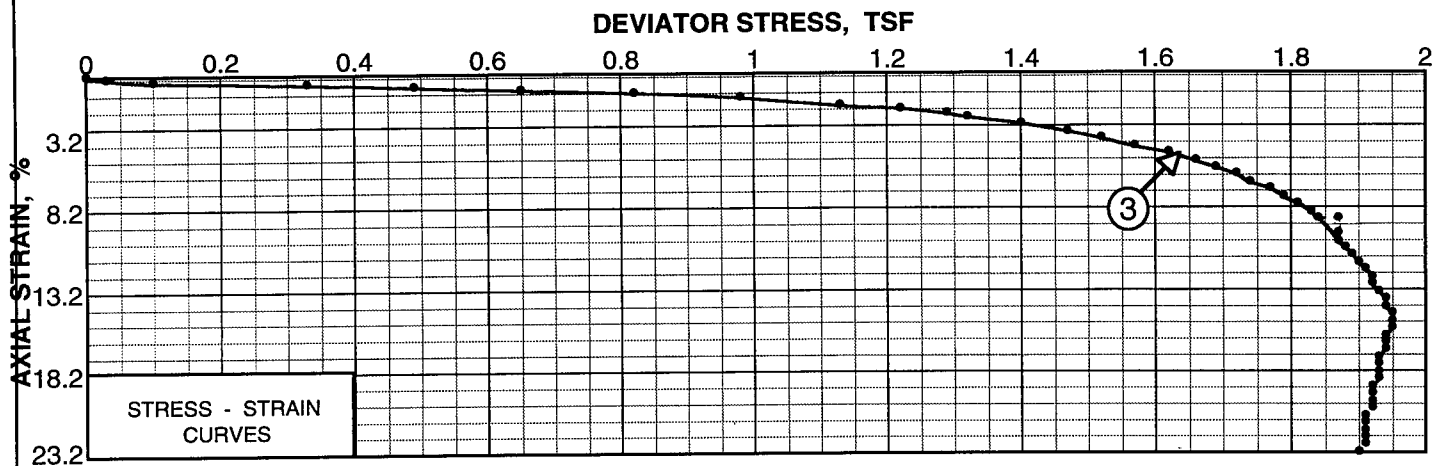
FILE NO.
8435A

SUMMARY OF STRENGTH TESTS

PLATE NO.

BORING NO. MR-43U

5



DESCRIPTION OF MATERIAL TESTED

DARK GRAY GREEN SLIGHTLY ORGANIC MICACEOUS SILTY FINE SAND,
TRACE CLAY, CLAY SEAMS, MEDIUM TO COARSE SAND, SHELLS
STRATUM (ES)

SYMBOLS FOR TEST TYPES

Q - UNCONSOLIDATED UNDRAINED
TRIAXIAL SHEAR TEST

KEY	BORING NO.	SAMPLE NO.	SOIL TYPE	TEST TYPE	LATERAL PRESSURE TSF	WATER CONTENT-%		DEGREE OF SATURATION-%		DEVIATOR STRESS TSF	AXIAL STRAIN %
						INITIAL	FINAL	INITIAL	FINAL		
1	MR-45U	6U	SM	Q	0.50	38	38			1.48	22
2	MR-45U	6U	SM	Q	1.0	36	37			1.03	2
3	MR-45U	6U	SM	Q	2.0	36	37			1.94	15
4	MR-43U	9U BOT	SM	Q	0.99	34	34			1.61	20

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MADE BY: MC
CH'KD BY: AAA

DATE: 5-27-98
DATE: 6-1-98

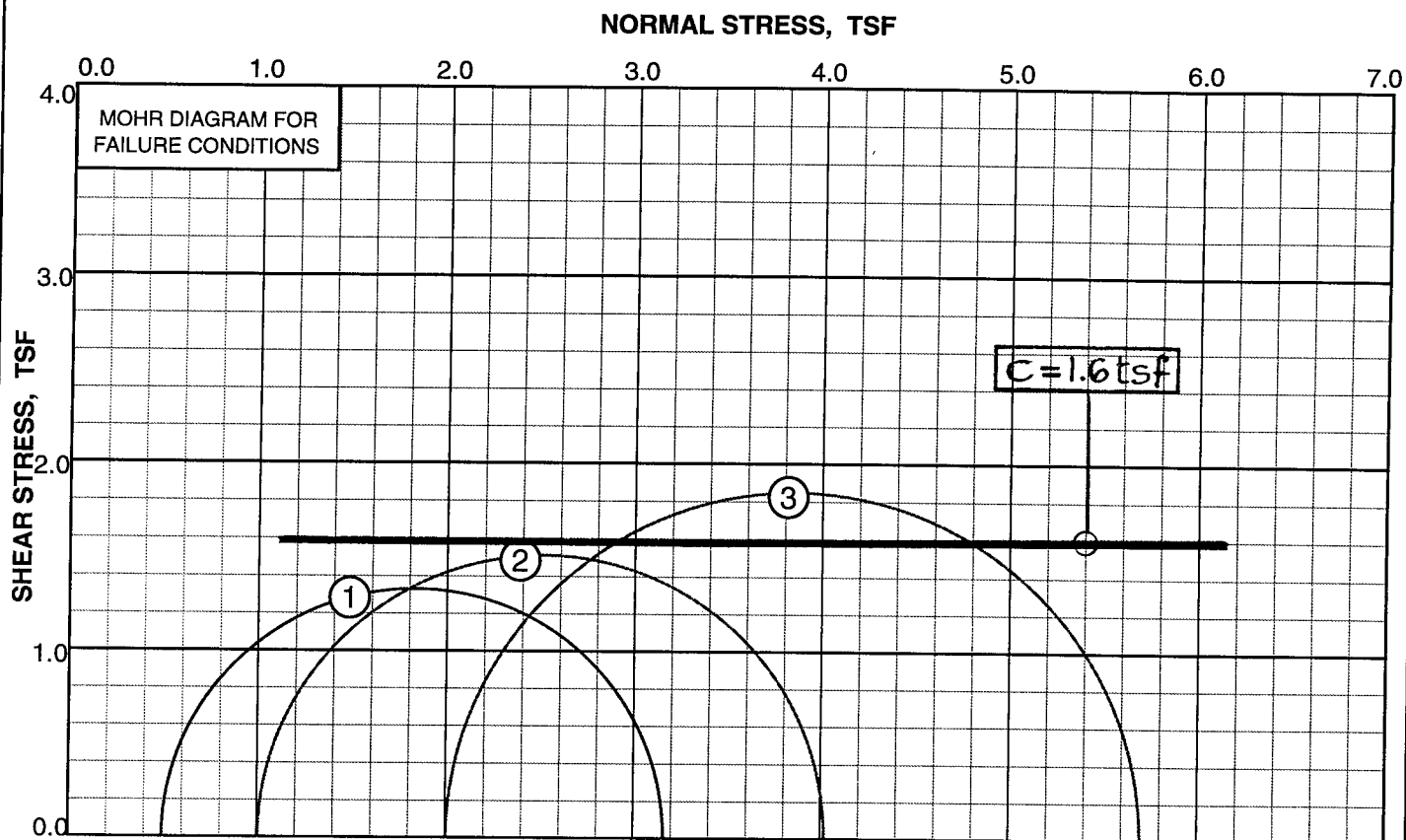
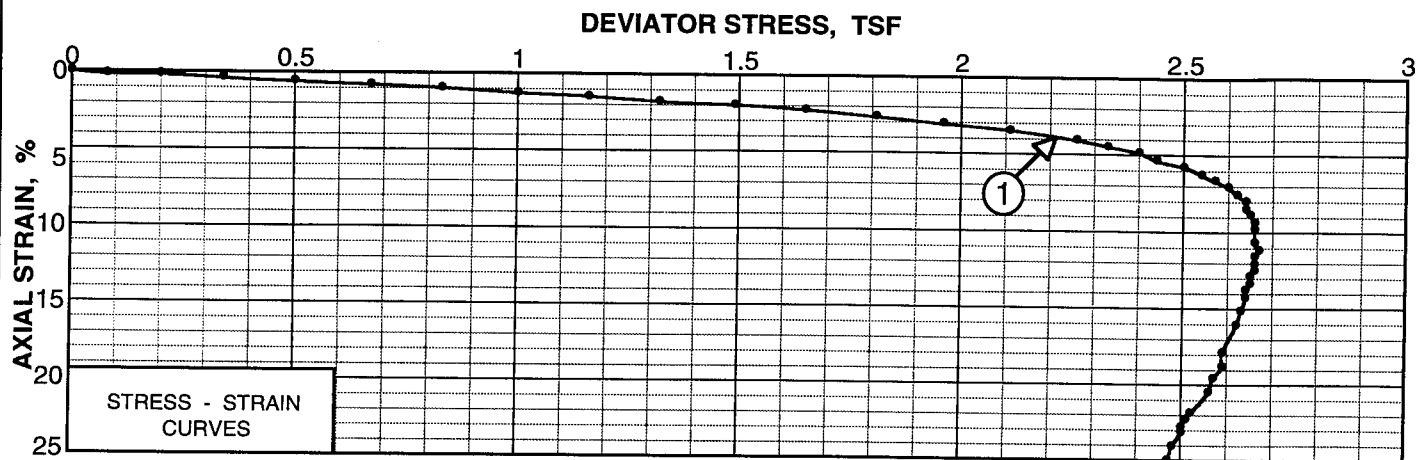
FILE NO.
8435A

SUMMARY OF STRENGTH TESTS

BORING NOS. MR-43U AND 45U

PLATE NO.

6



DESCRIPTION OF MATERIAL TESTED											SYMBOLS FOR TEST TYPES						
GRAY FINE SAND, TRACE SILT AND DARK GRAY SLIGHTLY ORGANIC MICACEOUS SILTY FINE SAND, TRACE CLAY, SHELLS, SHELL LAYERS STRATUM (MS)											Q - UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST						
KEY	BORING NO.	SAMPLE NO.	SOIL TYPE	TEST TYPE	LATERAL PRESSURE TSF	WATER CONTENT-%		DEGREE OF SATURATION-%		DEVIATOR STRESS TSF				AXIAL STRAIN %			
						INITIAL	FINAL	INITIAL	FINAL								
1	MR-45U	10U	SP-SM	Q	0.50	25	26			2.66				11			
2	MR-45U	10U	SP-SM	Q	1.0	24	25			3.02	6	WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY DE LEUW, CATHER & COMPANY GENERAL ENGINEERING CONSULTANTS					
3	MR-45U	13U	SM-SC	Q	2.0	26	27			3.70	7						
											MUESER RUTLEDGE CONSULTING ENGINEERS 708 THIRD AVENUE, NEW YORK, N.Y. 10017						
											MADE BY: MC		DATE: 5-27-98		FILE NO.		
											CH'KD BY: AAA		DATE: 6-1-98		8435A		
											SUMMARY OF STRENGTH TESTS					PLATE NO.	
											BORING NO. MR-45U					7	

CBR TEST DATA

SYMBOL	○	□	△
TEST PIT NO.	TP-2	TP-3	TP-6
CONDITION OF SAMPLE	SOAKED	SOAKED	SOAKED
SWELL IN % OF INITIAL HEIGHT	0.0	0.4	0.2
DRY DENSITY - PCF AT COMPACTION	112.8	110.0	106.7
DRY DENSITY - PCF AFTER SOAKING	112.1	110.0	106.7
WATER CONTENT- % AT COMPACTION	14.7	16.4	17.5
WATER CONTENT- % AFTER SOAKING	16.2	18.5	18.3
CALIFORNIA BEARING RATIO - %	10.2	10.8	14.6

PENETRATION RESISTANCE IN PSI

700.0

600.0

500.0

400.0

300.0

200.0

100.0

0.0

PENETRATION IN INCHES

0

0.1

0.2

0.3

0.4

0.5

0.6

NOTES:

1. FOR COMPACTION TEST DATA, SEE PLATE NO. 9
2. FOR GRAIN SIZE DISTRIBUTION CURVE, SEE PLATE NO. 3

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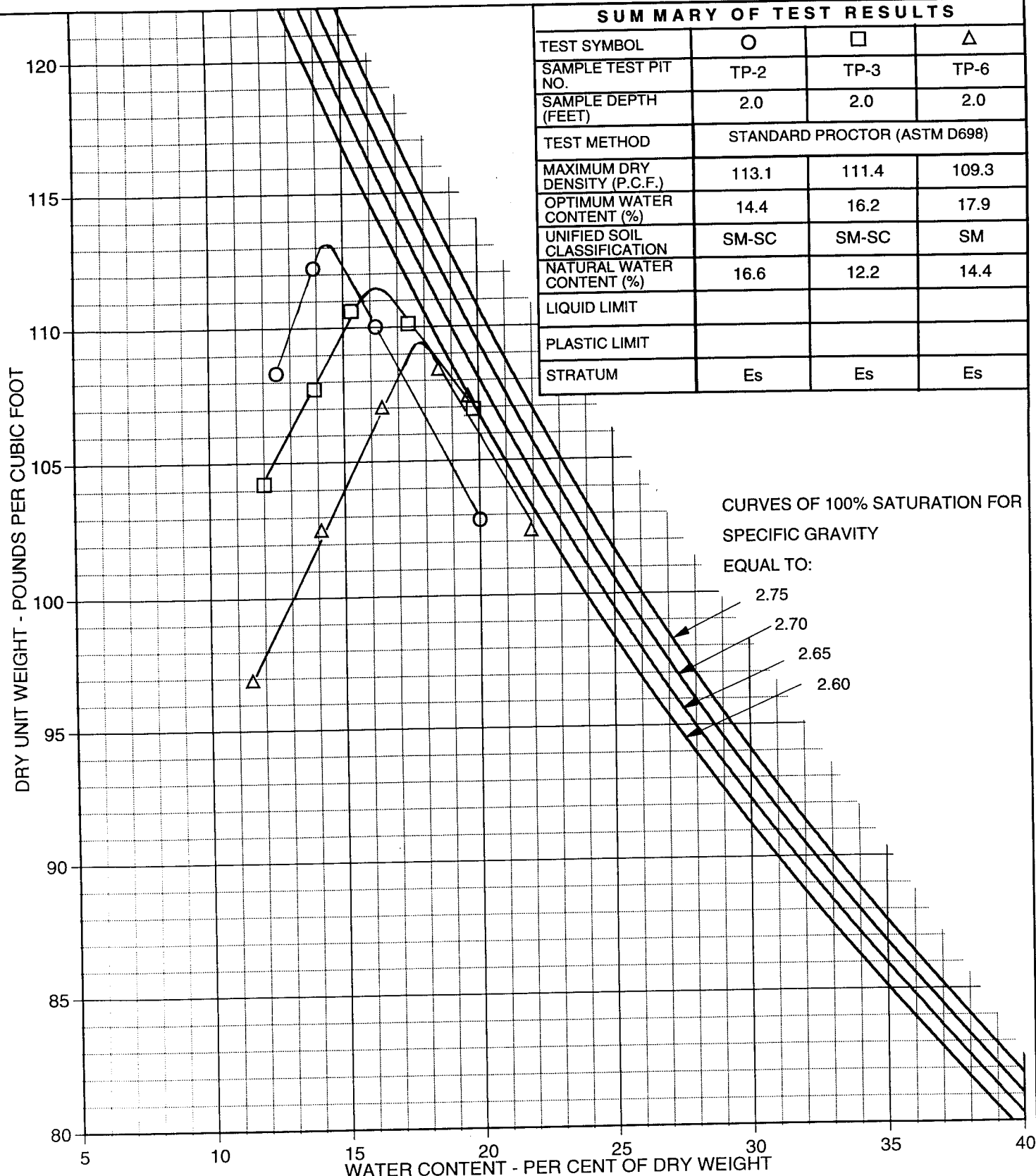
MADE BY: WEK
CH'KD BY: FW

DATE: 6-4-98
DATE: 6-5-98

FILE NO.
8435

CBR TEST RESULTS

PLATE NO.
8

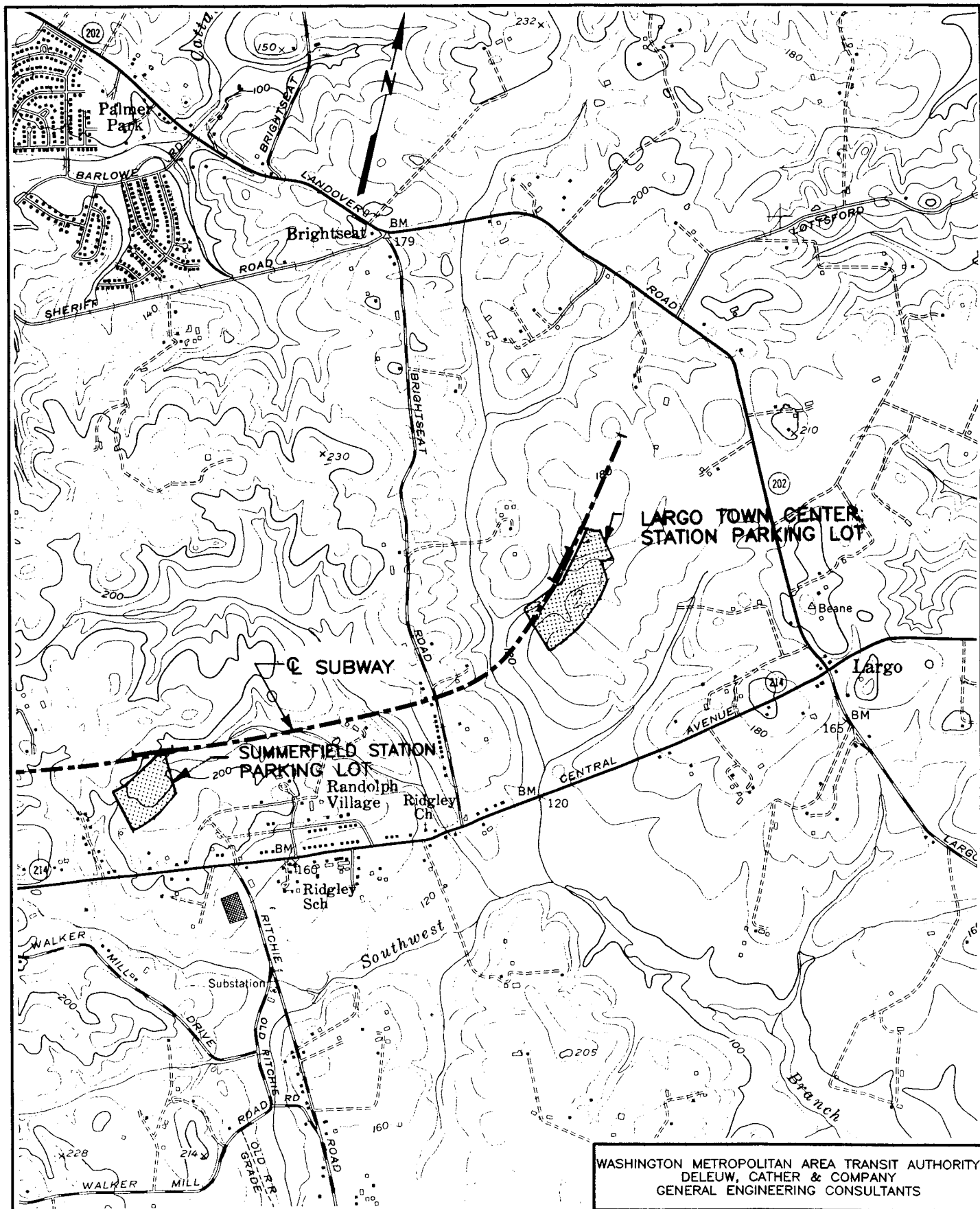


SUMMARY OF TEST RESULTS			
TEST SYMBOL	○	□	△
SAMPLE TEST PIT NO.	TP-2	TP-3	TP-6
SAMPLE DEPTH (FEET)	2.0	2.0	2.0
TEST METHOD	STANDARD PROCTOR (ASTM D698)		
MAXIMUM DRY DENSITY (P.C.F.)	113.1	111.4	109.3
OPTIMUM WATER CONTENT (%)	14.4	16.2	17.9
UNIFIED SOIL CLASSIFICATION	SM-SC	SM-SC	SM
NATURAL WATER CONTENT (%)	16.6	12.2	14.4
LIQUID LIMIT			
PLASTIC LIMIT			
STRATUM	Es	Es	Es

CURVES OF 100% SATURATION FOR
SPECIFIC GRAVITY
EQUAL TO:

2.75
2.70
2.65
2.60

DESCRIPTION OF TESTS					WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY DeLEUW, CATHER AND COMPANY GENERAL ENGINEERING CONSULTANTS			
TEST METHODS	STANDARD PROCTOR	MODIFIED PROCTOR	HARVARD MINIATURE					
VOLUME OF CYLINDER (CU. FT.)	1/30	1/30	1/454		MUESER RUTLEDGE CONSULTING ENGINEERS 708 THIRD AVENUE, NEW YORK, N.Y. 10017			
HAMMER WEIGHT (LBS.)	5 1/2	10	SPRING LB					
HAMMER DROP (IN.)	12	18	—		SCALE ---	MADE BY: MC	DATE: 6-8-98	FILE NO. 8435A
HAMMER BLOWS PER LAYER	25	25	TAMPS		CH'KD BY:	DATE:		
NUMBER OF LAYERS	3	5			COMPACTION DIAGRAM			PLATE NO.
COMPACTION ENERGY (FT. LBS. PER CU. FT.)	12,400	56,300			TEST PITS NOS. TP-2, TP-3 & TP-6			9



PORTION OF MAP TITLED:
USGS LANHAM QUADRANGLE
CONTOUR INTERVAL 20FT-
MEAN SEA LEVEL DATUM

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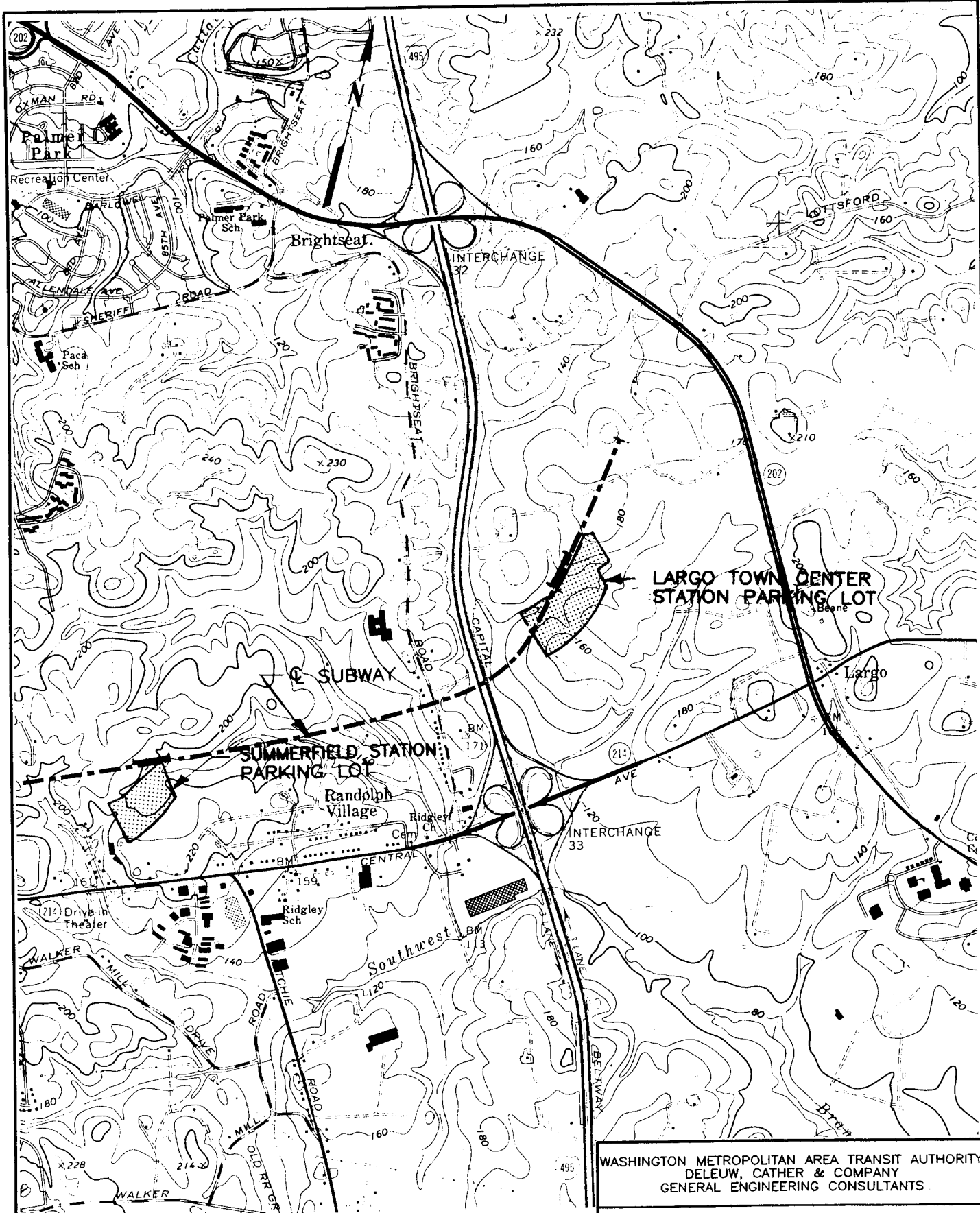
708 THIRD AVENUE, NEW YORK, N.Y. 10017

SCALE	MADE BY A.P.	DATE 6-98	FILE NO.
1"=2000'	CH'KD BY S.L.T.	DATE 6-98	8435a

TOPOGRAPHIC SURVEY
OF SITE - 1957

DRAWING NO.

SK-1



PORTION OF MAP TITLED:
USGS LANHAM QUADRANGLE
CONTOUR INTERVAL 20FT—
MEAN SEA LEVEL DATUM

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SCALE 1"=2000'	MADE BY A.P.	DATE 6-98	FILE NO. 8435a
	CH'D BY S.L.T.	DATE 6-98	

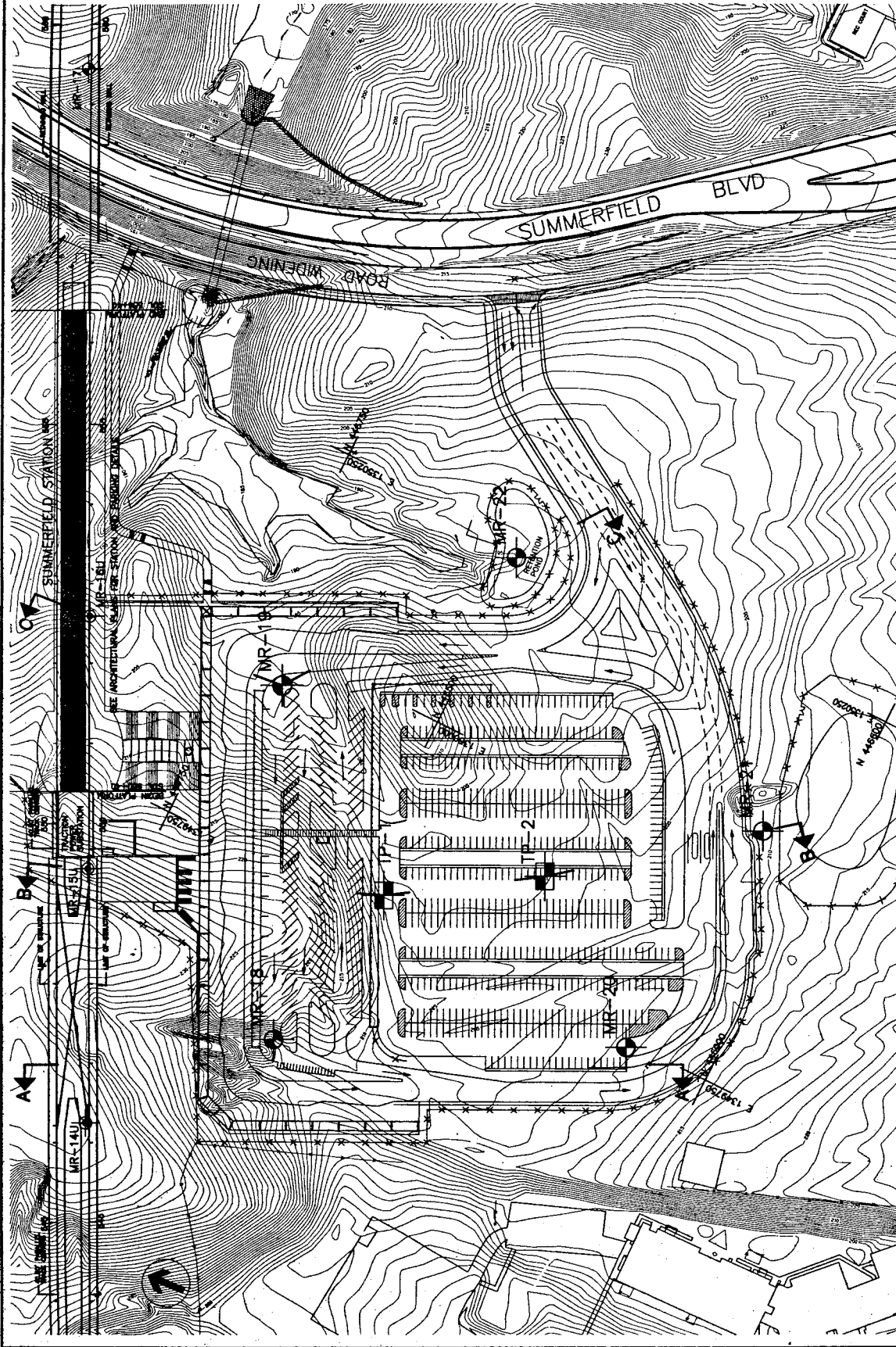
TOPOGRAPHIC SURVEY
OF SITE - 1971

DRAWING NO.

SK-2

LEGEND

- 2 1/2" AND 3 1/2" DIA. MR-SERIES DRY SAMPLE BORINGS
- 3 1/2" DIA. MR-SERIES OBSERVATION WELLS (BORINGS MADE AS PART OF THE CURRENT INVESTIGATION)
- 3 1/2" DIA. MR-SERIES BORINGS WITH UNDISTURBED SAMPLING AND OR OBSERVATION WELLS (BORINGS MADE AS PART OF THE CURRENT INVESTIGATION)
- TEST PIT MADE AS PART OF THE CURRENT INVESTIGATION
- BORINGS MADE FOR THIS INVESTIGATION



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HARRY WESSE & ASSOCIATES
GENERAL ARCHITECTURAL CONSULTANT



REFERENCE DRAWING

DATE	BY	DESCRIPTION
11/12/88	...	...
...	...	...
...	...	...
...	...	...
...	...	...

DESIGNED BY: ...
DRAWN BY: ...
CHECKED BY: ...
APPROVED BY: ...

ADDITION ROUTE

SUMMERFIELD STATION PARKING LOT
BORING AND TEST PIT LOCATION PLAN

SCALE: 0' 60' 120'

GPB-SO-290

GENERAL STRATA DESCRIPTIONS

STRATUM 1 (CALVERT) PLASTIC CLAY, SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF DARK GRAY, BROWN, OR CLAYEY SILT. TRACE FINE SAND, GRAVEL.

STRATUM 2 (CALVERT) FINE SAND, TRACE TO SOME SILT, CLAY. DARK GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. SAND, TRACE TO SOME SILT, CLAY AND SILTY OR CLAYEY FINE SAND, TRACE GRAVEL.

STRATUM 3 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 4 (AQUA) SILTY AND CLAYEY FINE SAND. LOOSE TO MEDIUM COMPACT GRAY GREEN, OLIVE GRAY SILTY AND CLAYEY FINE SAND, TRACE SHELLS WITH OCCASIONAL SLIGHTLY ORGANIC SILTY AND CLAYEY FINE SAND LAYERS.

STRATUM 5 (MONMOUTH) SLIGHTLY ORGANIC MEDIUM FINE SANDY SILTY AND CLAYEY SILT. LOOSE TO VERY COMPACT DARK GRAY OR OLIVE GREEN. TRACE TO SOME SILT, CLAY AND SILTY OR CLAYEY FINE SAND, TRACE GRAVEL.

STRATUM 6 (MONMOUTH) SLIGHTLY ORGANIC MEDIUM FINE SANDY SILTY AND CLAYEY SILT. LOOSE TO VERY COMPACT DARK GRAY OR OLIVE GREEN. TRACE TO SOME SILT, CLAY AND SILTY OR CLAYEY FINE SAND, TRACE GRAVEL.

STRATUM 7 (AQUA) PLASTIC CLAY, SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 8 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 9 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 10 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 11 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 12 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 13 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 14 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 15 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 16 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

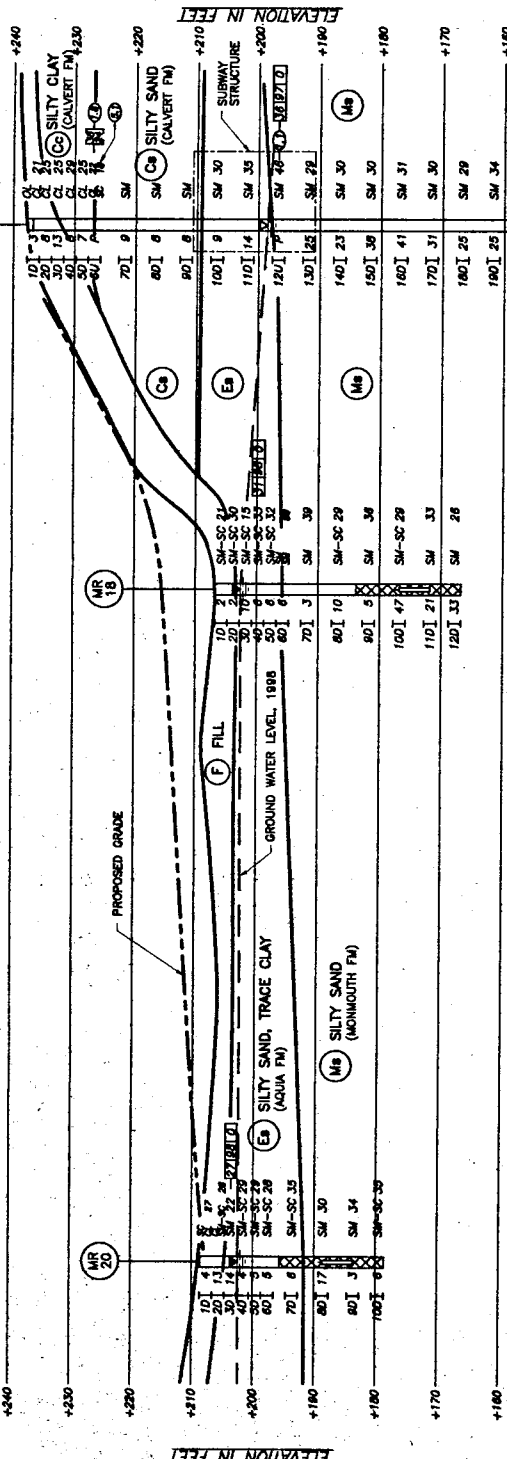
STRATUM 17 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 18 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

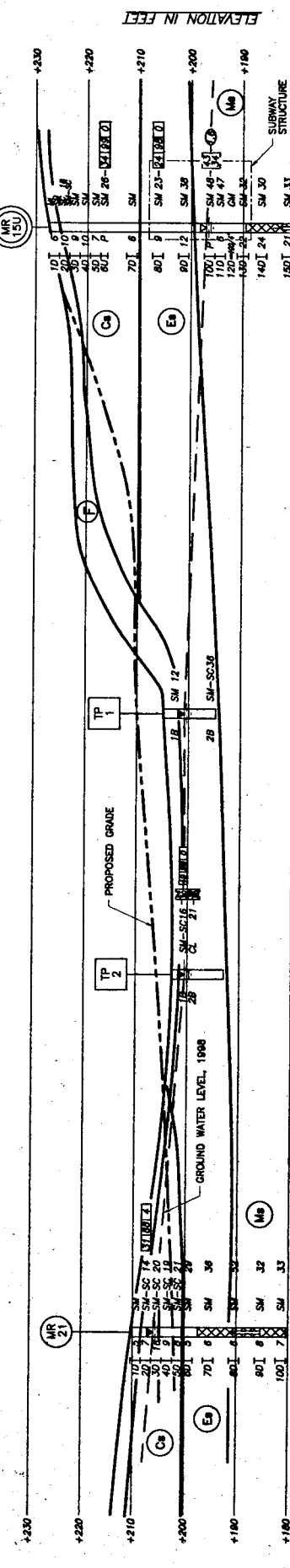
STRATUM 19 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 20 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.

STRATUM 21 (AQUA) PLASTIC TO SILTY AND SANDY CLAY OR CLAYEY SILT. MEDIUM TO STIFF GRAY OR OLIVE GREEN. LOOSE TO MEDIUM COMPACT. CLAY TO SILTY AND SANDY CLAY OR CLAYEY SILT. TRACE LIGNITE WITH OCCASIONAL SLIGHTLY ORGANIC FINE SANDY AND SILTY CLAY LAYERS, TRACE SHELLS.



SECTION A-A



SECTION B-B

PERCENT OF MATERIAL RETAINED ON NO. 40 SIEVE SIZE
PERCENT OF MATERIAL PASSING THE NO. 40 SIEVE SIZE
PERCENT OF MATERIAL PASSING THE NO. 200 SIEVE SIZE

INDICATES POSITION OF POROUS INTAKE IN THE OBSERVATION WELL

LEGEND

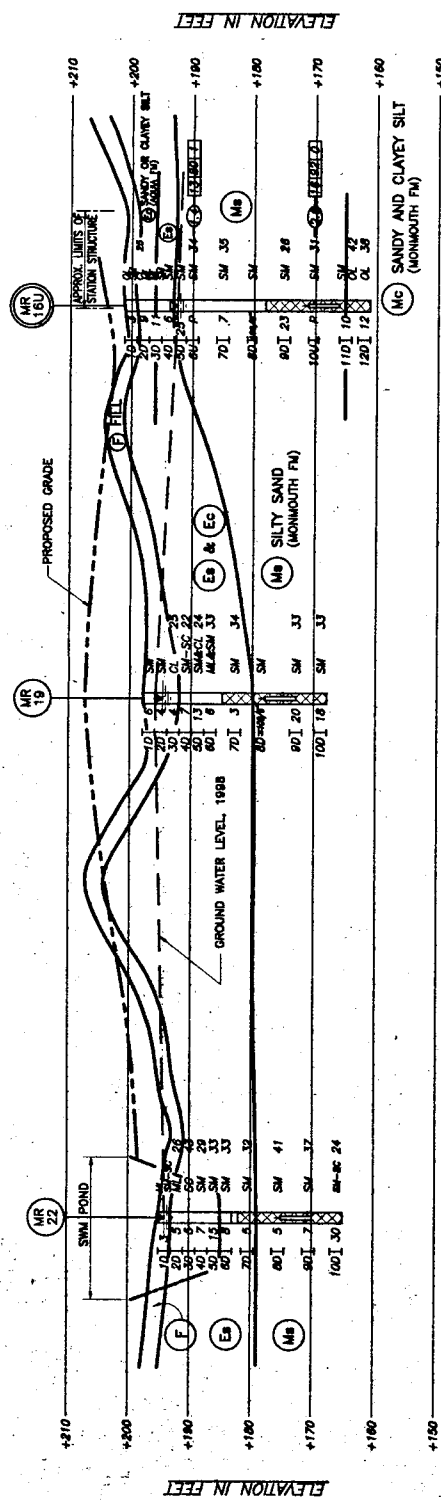
DESIGNED	DATE	BY	DESCRIPTION
DRAWN	DATE	BY	DESCRIPTION
CHECKED	DATE	BY	DESCRIPTION
APPROVED	DATE	BY	DESCRIPTION



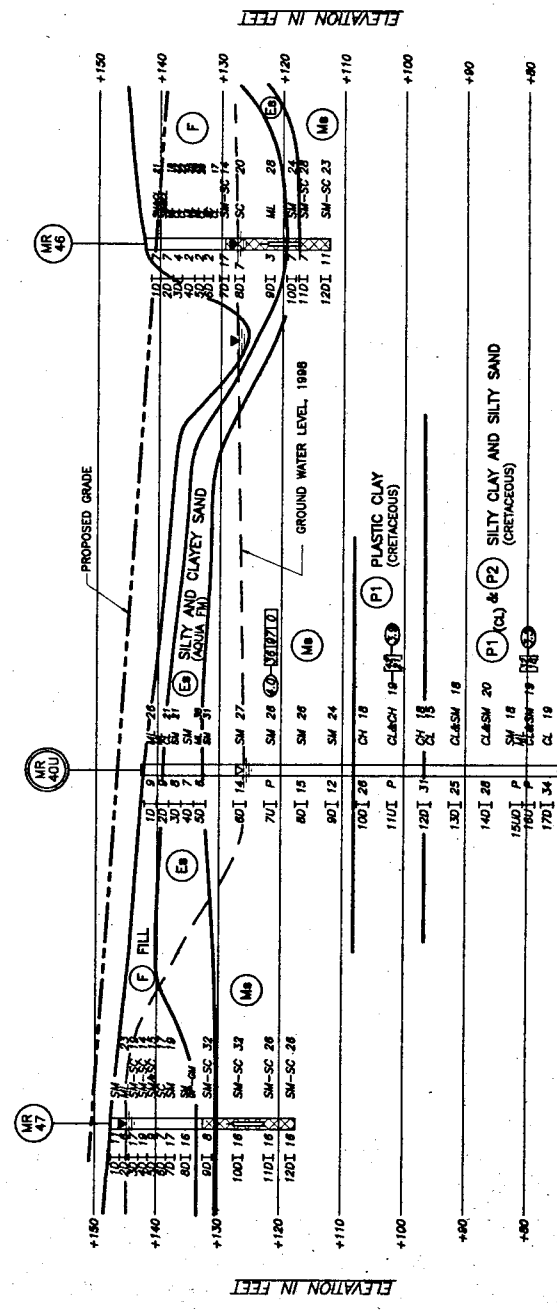
WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY
MESSER RUTLEDGE CONSULTING ENGINEERING
708 THIRD AVENUE, NEW YORK, N.Y. 10017
SUBMITTED: *[Signature]*

DE LEON, CATER & COMPANY
GENERAL ENGINEERING CONSULTANT
HARRY WEEBE & ASSOCIATES
GENERAL ARCHITECTURAL CONSULTANT

ADDISON ROUTE
SUMMERFIELD STATION PARKING LOT
GEOLOGICAL SECTIONS A-A AND B-B
SCALE: 1" = 40'
DATE: 10/1/68
BY: *[Signature]*
NOT: *[Signature]*
GFG-SO-320

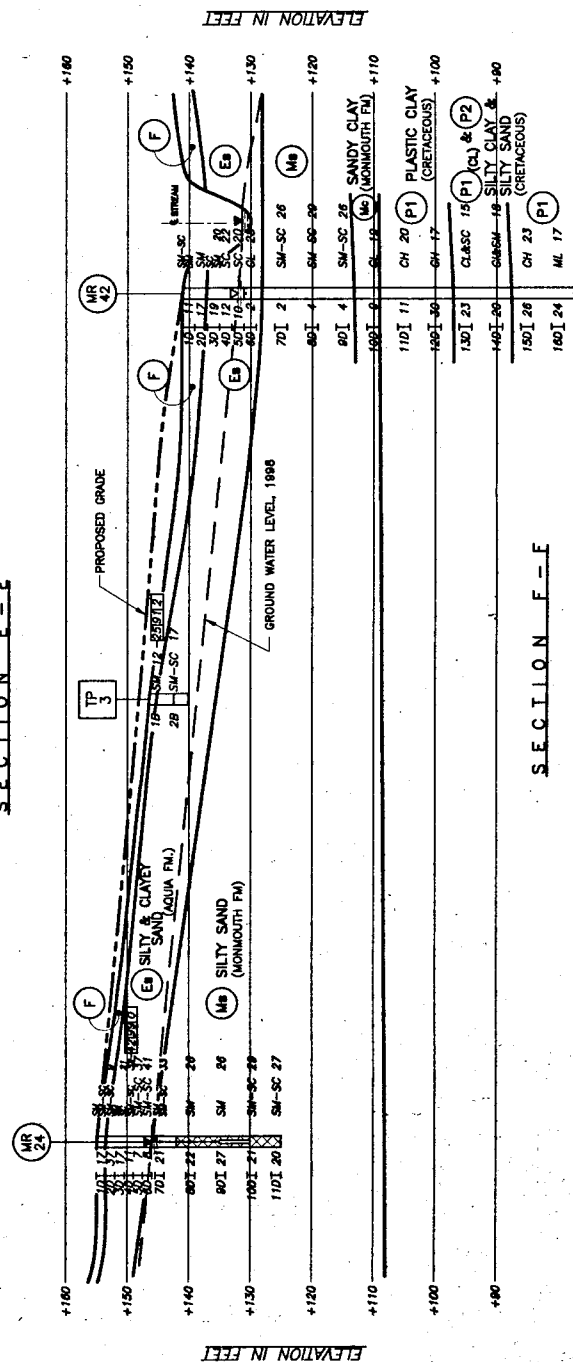
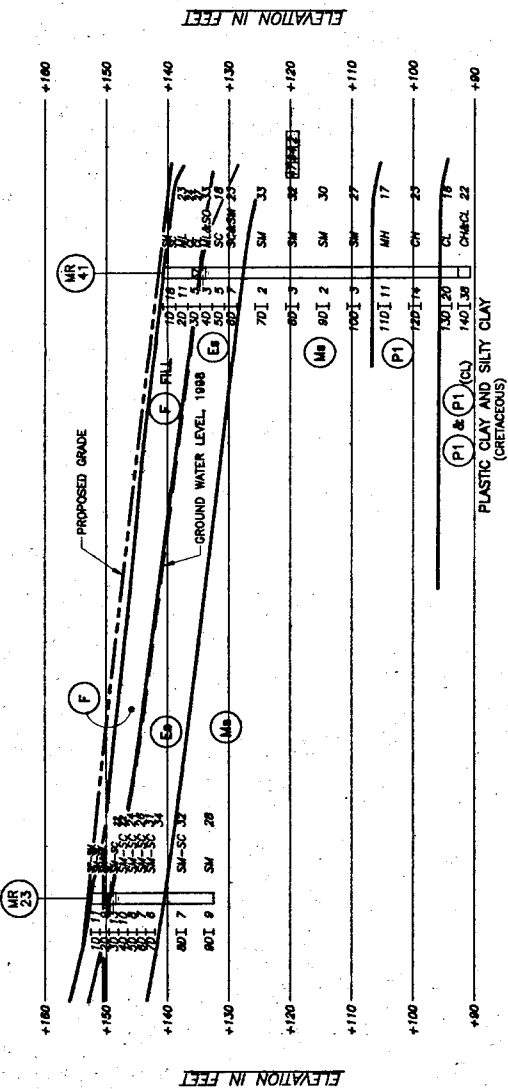


SECTION C-C



SECTION D-D

DRAWN: <u>NY/AP</u> DATE: <u>6-28</u> CHECKED: <u>BSL</u> DATE: <u>6-28</u> APPROVED: _____		REFERENCE DRAWING NO. 1-1 DESCRIPTION: <u>GENERAL NOTES, LEGEND AND SYMBOLS</u> NO. 2-1 DESCRIPTION: <u>STATIONS AND TIE IN LOCATIONS</u> NO. 3-1 DESCRIPTION: <u>STATIONS AND TIE IN LOCATIONS</u>		REVISIONS NO. 1 DATE: _____ BY: _____ DESCRIPTION: _____	
WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY DE LEON, CUTLER & COMPANY GENERAL ENGINEERING CONSULTANT HARRY WEBER & ASSOCIATES GENERAL ARCHITECTURAL CONSULTANT					
ADDISON ROUTE SUMMERFIELD AND LARGO TOWN CENTER STATIONS PARKING LOTS GEOLOGICAL SECTIONS C-C AND D-D SCALE: HORIZ. 1" = 40' VERT. 1" = 20' GPG-SO-330					



WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY DE LEM, GATHER & COMPANY GENERAL ENGINEERING CONSULTANT HARRY WEISE & ASSOCIATES GENERAL ARCHITECTURAL CONSULTANT		ADDISON ROUTE LARGO TOWN CENTER STATION PARKING LOT GEOLOGICAL SECTIONS E-E AND F-F	
DRAWN: J. L. J. CHECKED: H. L. J. APPROVED: J. L. J.		SCALE: 1" = 10' HORIZ. 1" = 10' VERT. GPG-SO-340	

[illegible]

- NOTES:
- BORINGS NO. 18 THROUGH NO. 21, MR. 22 THROUGH MR. 25, GEORGE'S CORPORATION UNDER CONTRACT TO THE DISTRICT OF COLUMBIA, WASHINGTON, D.C., ON APRIL 20, 1968. THE BORINGS WERE INSPECTED AND LOGGED BY GEORGE'S CORPORATION.
 - TEST PITS NOS. 18, 19, 20, 21, 22, 23, 24, 25, WERE MADE BY GEORGE'S CORPORATION. THE BORINGS WERE INSPECTED AND LOGGED BY GEORGE'S CORPORATION.
 - BORING NO. 18, 19, 20, 21, 22, 23, 24, 25, WERE MADE BY GEORGE'S CORPORATION. THE BORINGS WERE INSPECTED AND LOGGED BY GEORGE'S CORPORATION.
 - LOCATIONS OF THE BORINGS ARE LISTED ON MAP NO. 1 OF THE BORING LOGS.

BORING NUMBER MR-21

Ground surface elevation +210.4

DEPTH BELOW GROUND SURFACE, FEET	LOG	DESCRIPTION	LOG	DESCRIPTION
0	10	12.33	10	12.33
1	11	12.33	11	12.33
2	12	12.33	12	12.33
3	13	12.33	13	12.33
4	14	12.33	14	12.33
5	15	12.33	15	12.33
6	16	12.33	16	12.33
7	17	12.33	17	12.33
8	18	12.33	18	12.33
9	19	12.33	19	12.33
10	20	12.33	20	12.33
11	21	12.33	21	12.33
12	22	12.33	22	12.33
13	23	12.33	23	12.33
14	24	12.33	24	12.33
15	25	12.33	25	12.33
16	26	12.33	26	12.33
17	27	12.33	27	12.33
18	28	12.33	28	12.33
19	29	12.33	29	12.33
20	30	12.33	30	12.33

Boring started 4:30-48
 Final depth 30.0
 Casing depth 4.0
 Average depth of ground water observed in the boring 4.0
 REMARKS:
 Used 140 lb. automatic hammer to drive 2-inch O.D. split spoon sampler.
 Used water below 4' depth to maintain hole open.
 Observation well consisting of 1-1/2" PVC pipe installed with top at 25' depth.
 Borehole was grouted between 0' and 10' depth.

BORING NUMBER MR-20

Ground surface elevation +208.5

DEPTH BELOW GROUND SURFACE, FEET	LOG	DESCRIPTION	LOG	DESCRIPTION
0	10	12.33	10	12.33
1	11	12.33	11	12.33
2	12	12.33	12	12.33
3	13	12.33	13	12.33
4	14	12.33	14	12.33
5	15	12.33	15	12.33
6	16	12.33	16	12.33
7	17	12.33	17	12.33
8	18	12.33	18	12.33
9	19	12.33	19	12.33
10	20	12.33	20	12.33
11	21	12.33	21	12.33
12	22	12.33	22	12.33
13	23	12.33	23	12.33
14	24	12.33	24	12.33
15	25	12.33	25	12.33
16	26	12.33	26	12.33
17	27	12.33	27	12.33
18	28	12.33	28	12.33
19	29	12.33	29	12.33
20	30	12.33	30	12.33

Boring started 4:30-48
 Final depth 30.0
 Casing depth 4.0
 Average depth of ground water observed in the boring 4.0
 REMARKS:
 Used 140 lb. automatic hammer to drive 2-inch O.D. split spoon sampler.
 Used water below 4' depth to maintain hole open.
 Observation well consisting of 1-1/2" PVC pipe installed with top at 25' depth.
 Borehole was grouted between 0' and 10' depth.

BORING NUMBER MR-19

Ground surface elevation +187.8

DEPTH BELOW GROUND SURFACE, FEET	LOG	DESCRIPTION	LOG	DESCRIPTION
0	10	12.33	10	12.33
1	11	12.33	11	12.33
2	12	12.33	12	12.33
3	13	12.33	13	12.33
4	14	12.33	14	12.33
5	15	12.33	15	12.33
6	16	12.33	16	12.33
7	17	12.33	17	12.33
8	18	12.33	18	12.33
9	19	12.33	19	12.33
10	20	12.33	20	12.33
11	21	12.33	21	12.33
12	22	12.33	22	12.33
13	23	12.33	23	12.33
14	24	12.33	24	12.33
15	25	12.33	25	12.33
16	26	12.33	26	12.33
17	27	12.33	27	12.33
18	28	12.33	28	12.33
19	29	12.33	29	12.33
20	30	12.33	30	12.33

Boring started 4:30-48
 Final depth 30.0
 Casing depth 4.0
 Average depth of ground water observed in the boring 4.0
 REMARKS:
 Used 140 lb. automatic hammer to drive 2-inch O.D. split spoon sampler.
 Used water below 4' depth to maintain hole open.
 Observation well consisting of 1-1/2" PVC pipe installed with top at 25' depth.
 Borehole was grouted between 0' and 10' depth.

BORING NUMBER MR-18

Ground surface elevation +208.5

DEPTH BELOW GROUND SURFACE, FEET	LOG	DESCRIPTION	LOG	DESCRIPTION
0	10	12.33	10	12.33
1	11	12.33	11	12.33
2	12	12.33	12	12.33
3	13	12.33	13	12.33
4	14	12.33	14	12.33
5	15	12.33	15	12.33
6	16	12.33	16	12.33
7	17	12.33	17	12.33
8	18	12.33	18	12.33
9	19	12.33	19	12.33
10	20	12.33	20	12.33
11	21	12.33	21	12.33
12	22	12.33	22	12.33
13	23	12.33	23	12.33
14	24	12.33	24	12.33
15	25	12.33	25	12.33
16	26	12.33	26	12.33
17	27	12.33	27	12.33
18	28	12.33	28	12.33
19	29	12.33	29	12.33
20	30	12.33	30	12.33

Boring started 4:30-48
 Final depth 30.0
 Casing depth 4.0
 Average depth of ground water observed in the boring 4.0
 REMARKS:
 Used 140 lb. automatic hammer to drive 2-inch O.D. split spoon sampler.
 Used water below 4' depth to maintain hole open.
 Observation well consisting of 1-1/2" PVC pipe installed with top at 25' depth.
 Borehole was grouted between 0' and 10' depth.

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY
 DE LEWIS, CATHY & COMPANY
 GENERAL ENGINEERING CONSULTANTS
 HARRY WISSE & ASSOCIATES
 GENERAL ARCHITECTURAL CONSULTANT
 APPROVED



REVISIONS	DATE	BY	DESCRIPTION
1			
2			
3			
4			
5			
6			
7			
8			
9			
10			

ADDISON ROUTE
 LOGS OF MR-SERIES BORINGS
 MR-18 TO MR-21

SCALE
 0 3 6 12
 FEET
 GPG-50-360

[illegible]

Boundaries were ground between 0° and 15° depth.

[illegible]

TEST PIT NUMBER TP-1

Ground surface elevation: 204.8

Material Description	Depth
Topsoil: Dark brown organic fine sandy silty loam (F5) (R4)	0.0
8-10 Brown silty fine sand, trace gravel, roots (F5) (R4)	2.0
8-12 Medium gray brown silty fine sand, trace clay, clay pockets, roots (R4) (C2)	10.0

Test Pit started 8-7-98

Final depth: 10.0

Remarks:

Test pit was excavated with a backhoe loader. Bottom of pit was at 10.0 feet below ground surface. Pit was excavated to a depth of 10.0 feet. Pit was backfilled with topsoil.

TEST PIT NUMBER TP-2

Ground surface elevation: 191.5

Material Description	Depth
Topsoil: Dark brown organic fine sandy silty loam (F5) (R4)	0.0
8-10 Brown silty fine sand, trace gravel, roots (F5) (R4)	2.0
8-12 Medium gray brown silty fine sand, trace clay, clay pockets, roots (R4) (C2)	10.0

Test Pit started 8-7-98

Final depth: 10.0

Remarks:

Test pit was excavated with a backhoe loader. Bottom of pit was at 10.0 feet below ground surface. Pit was excavated to a depth of 10.0 feet. Pit was backfilled with topsoil.

TEST PIT NUMBER TP-3

Ground surface elevation: 203.0

Material Description	Depth
Topsoil: Dark brown organic fine sandy silty loam (F5) (R4)	0.0
8-10 Brown silty fine sand, trace clay, gravel, medium to coarse sand (R4) (C2)	2.0
8-12 Medium gray brown silty clay, some fine sand, trace fine sandy silty loam (R4) (C2)	10.0

Test Pit started 8-7-98

Final depth: 10.0

Remarks:

Test pit was excavated with a backhoe loader. Bottom of pit was at 10.0 feet below ground surface. Pit was excavated to a depth of 10.0 feet. Pit was backfilled with topsoil.

TEST PIT NUMBER TP-4

Ground surface elevation: 192.1

Material Description	Depth
Topsoil: Dark brown organic fine sandy silty loam (F5) (R4)	0.0
8-10 Brown silty fine sand, trace roots (F5) (R4)	2.0
8-12 Medium gray brown silty fine sand, trace clay, clay pockets, roots (R4) (C2)	10.0

Test Pit started 8-7-98

Final depth: 10.0

Remarks:

Test pit was excavated with a backhoe loader. Bottom of pit was at 10.0 feet below ground surface. Pit was excavated to a depth of 10.0 feet. Pit was backfilled with topsoil.

TEST PIT NUMBER TP-5

Ground surface elevation: 146.5

Material Description	Depth
Topsoil: Dark brown organic fine sandy silty loam (F5) (R4)	0.0
8-10 Brown silty fine sand, trace roots (F5) (R4)	2.0
8-12 Medium gray brown silty fine sand, trace clay, clay pockets, roots (R4) (C2)	10.0

Test Pit started 8-7-98

Final depth: 10.0

Remarks:

Test pit was excavated with a backhoe loader. Bottom of pit was at 10.0 feet below ground surface. Pit was excavated to a depth of 10.0 feet. Pit was backfilled with topsoil.

TEST PIT NUMBER TP-6

Ground surface elevation: 146.5

Material Description	Depth
Topsoil: Dark brown organic fine sandy silty loam (F5) (R4)	0.0
8-10 Brown silty fine sand, trace roots (F5) (R4)	2.0
8-12 Medium gray brown silty fine sand, trace clay, clay pockets, roots (R4) (C2)	10.0

Test Pit started 8-7-98

Final depth: 10.0

Remarks:

Test pit was excavated with a backhoe loader. Bottom of pit was at 10.0 feet below ground surface. Pit was excavated to a depth of 10.0 feet. Pit was backfilled with topsoil.

REFERENCE DRAWINGS

NUMBER

DESCRIPTION

DATE

BY

REVISIONS



WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY

MUESER RUTLEDGE CONSULTING ENGINEERS

708 THIRD AVENUE, NEW YORK, N.Y. 10017

SUBMITTED

APPROVED

ADDISON ROUTE

LOGS OF TEST PITS

TP-1 TO TP-6

DRAWING NO.

GPG-SO-390

SCALE

0 1.5' 3'

APPENDIX

CORROSION AND CHEMICAL TESTS FOR THIS INVESTIGATION



RECEIVED MAY 28 1998

ARTECH TESTING, L.L.C.

14554 LEE ROAD • CHANTILLY, VA 20151-1632
703 378-7263 • 800 283-7848 • FAX 703 378-7274

May 26, 1998

Mr. Paul Chung
Geotech Engineers, Inc.
11890-U Old Baltimore Pike
Beltsville, Maryland 20705

PRODUCT TESTING

Subject: Analysis of Soil Samples

Reference: WMATA Boring Contract 212
ARTECH C80110A (re-issued to correct sample identifications)

FAILURE ANALYSIS

pH of Soil in Water at 25°C by EPA Method 9045C
Resistivity of Soil by CA DOT Method 643
Chloride and Sulfate by EPA Method 9056
Total Sulfur Content of Soil by Combustion/Iodometric Titration

LITIGATION SUPPORT

Sampled by: Geotech

CHEMICAL ANALYSIS

Sample ID	pH	Resistivity	Chloride	Sulfate	Total Sulfur
MR-45U/0.5-2.0'	7.40	12.55 kΩ-cm	3.19 mg/kg	10.80 mg/kg	< 5.0 mg/kg
MR-18/0-2.0'	4.75	1.57 kΩ-cm	3.02 mg/kg	< 2.00 mg/kg	35.7 mg/kg
MR-19/0-2.0'	4.10	810 Ω-cm	6.55 mg/kg	8.53 mg/kg	24.8 mg/kg
MR-20/4-6.0'	3.85	557 Ω-cm	1.15 mg/kg	18.69 mg/kg	88.2 mg/kg
MR-43U/0.5-2.0'	7.10	724 Ω-cm	139.55 mg/kg	62.39 mg/kg	560.7 mg/kg
MR-44/0.5-2.0'	10.15	646 Ω-cm	81.80 mg/kg	58.30 mg/kg	514.9 mg/kg

Notes: 1) Chloride and Sulfates results are for the water soluble ions.
2) Sample identifications changed per customer request. New sample identification does not match sample jars or chain of custody form for samples MR-45U, MR-43U and MR-44.

ENGINEERING CONSULTING

Sincerely,
ARTECH Testing, LLC

Karl Schweizer
Chemist

MATERIALS RESEARCH

BIOMATERIALS

FOOTWEAR TESTING

