

Federal Radionavigation Plan

JULY 1980



Volume III (of 4)
Radionavigation System Characteristics

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PREFACE

The Departments of Defense and Transportation developed this Federal Radionavigation Plan (FRP) to ensure efficient use of resources and full protection of national interests. The plan sets forth the Federal interagency approach to the implementation and operation of radionavigation systems.

Various existing and planned radionavigation systems used in air, land, and marine navigation are reviewed in terms of user requirements and current status. The FRP contents reflect a response to a unique combination:

- o DOT responsibilities for public safety and transportation economy
- o DOD responsibility for national security in normal and stressed situations.

This plan will be updated annually. The established DOD/DOT interagency management approach will enable continuing control and review of U.S. radionavigation systems.

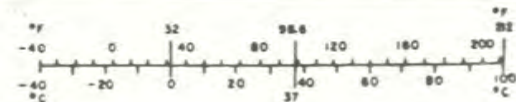
METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
in	inches	2.5	centimeters	cm
ft	feet	30	centimeters	cm
yd	yards	0.9	meters	m
mi	miles	1.6	kilometers	km
AREA				
in ²	square inches	6.5	square centimeters	cm ²
ft ²	square feet	0.09	square meters	m ²
yd ²	square yards	0.8	square meters	m ²
mi ²	square miles	2.6	square kilometers	km ²
acres	acres	0.4	hectares	ha
MASS (weight)				
oz	ounces	28	grams	g
lb	pounds	0.45	kilograms	kg
	short tons (2000 lb)	0.9	tonnes	t
VOLUME				
tsp	teaspoons	5	milliliters	ml
Tbsp	tablespoons	15	milliliters	ml
fl oz	fluid ounces	30	milliliters	ml
c	cups	0.24	liters	l
pt	pints	0.47	liters	l
qt	quarts	0.95	liters	l
gal	gallons	3.8	liters	l
ft ³	cubic feet	0.03	cubic meters	m ³
yd ³	cubic yards	0.76	cubic meters	m ³
TEMPERATURE (exact)				
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C

Approximate Conversions from Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
mm	millimeters	0.04	inches	in
cm	centimeters	0.4	inches	in
m	meters	3.3	feet	ft
km	kilometers	1.1	miles	mi
		0.6	miles	mi
AREA				
cm ²	square centimeters	0.16	square inches	in ²
m ²	square meters	1.2	square yards	yd ²
km ²	square kilometers	0.4	square miles	mi ²
ha	hectares (10,000 m ²)	2.5	acres	ac
MASS (weight)				
g	grams	0.035	ounces	oz
kg	kilograms	2.2	pounds	lb
t	tonnes (1000 kg)	1.1	short tons	st
VOLUME				
ml	milliliters	0.03	fluid ounces	fl oz
l	liters	2.1	pints	pt
l	liters	1.06	quarts	qt
l	liters	0.26	gallons	gal
m ³	cubic meters	36	cubic feet	ft ³
m ³	cubic meters	1.3	cubic yards	yd ³
TEMPERATURE (exact)				
°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature	°F



FEDERAL RADIONAVIGATION PLAN
VOLUME III
RADIONAVIGATION SYSTEM CHARACTERISTICS

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VOLUME III

CHAPTER 1

GENERAL

1.0 INTRODUCTION

This volume addresses the characteristics, capabilities, and limitations of existing and proposed major radionavigation systems. These systems are:

- | | | | |
|---|----------------------|---|--------------|
| o | LORAN-A | o | Radiobeacons |
| o | LORAN-C | o | ILS |
| o | VOR, VOR/DME, VORTAC | o | MLS |
| o | OMEGA | o | NAVSTAR GPS |
| o | TACAN | o | TRANSIT. |

VOLUME III

CHAPTER 2

RADIONAVIGATION SYSTEM PARAMETERS

2.0 SYSTEM PERFORMANCE PARAMETERS - DEFINITIONS

All of the systems considered are defined in terms of system performance parameters which determine the utilization and limitations of the individual navigation systems. These parameters are:

- | | | | |
|---|------------------------|---|---------------|
| o | Signal Characteristics | o | Fix Rate |
| o | Accuracy | o | Fix Dimension |
| o | Availability | o | Capacity |
| o | Coverage | o | Ambiguity. |
| o | Reliability | | |

2.1 SIGNAL CHARACTERISTICS

These parameters, which characterize the signal in space, are principally signal power levels, frequencies, signal formats, data rates, and any other data sufficient to completely define the means by which a user derives navigational information.

2.2 ACCURACY

In navigation, the accuracy of an estimated or measured position of a craft (vehicle, aircraft, or vessel) at a given time is the degree of conformance of that position with the true position of the craft at that time. Since accuracy is a statistical measure of performance, a statement of the accuracy of a navigation system is meaningless unless it includes a statement of the uncertainty in position which applies.

2.2.1 Statistical Measure of Accuracy*

Navigation system errors generally follow a known error distribution. Therefore, the uncertainty in position can be expressed as the probability that the error will not exceed a certain amount. A thorough treatment of errors is complicated by the fact that the total error is comprised of errors caused by instability of the transmitted signal, effects of weather and other physical changes in the propagation medium, errors in the receiving equipment, and errors introduced by the human navigator. In specifying, or describing the accuracy of a system, the human errors usually are excluded. Further complications arise because some navigation

*Reference - Mathematical Considerations Pertaining to the Accuracy of Position Location and Navigation Systems - Part I; W. Allan Burt, et al; Stanford Research Institute April 1966, (NTIS - AD 629 609).

systems are linear (one-dimensional) while others provide two or three dimensions of position. When specifying linear accuracy, or when it is necessary to specify requirements in terms of orthogonal axes, e.g., along-track or cross-track, the 95 percent confidence level will be used. When two or three dimensional accuracies are used, the 2 drms (distance root mean squared) uncertainty estimate will be used. 2 drms is the radius of a circle that contains at least 95% of all possible fixes that can be obtained with a system at any one place. DOD specifies horizontal accuracy in terms of Circular Error Probable (CEP--the radius of a circle containing 50% of all possible fixes). For the FRP, it is agreed that the conversion of CEP to 2 drms would be accomplished by using 2.5 as the multiplier.

2.2.2 Types of Accuracy

Specifications of radionavigation system accuracy generally refer to one or more of the following definitions:

- A. Predictable Accuracy: The accuracy of a position with respect to the geographic, or geodetic, coordinates of the earth.
- B. Repeatable Accuracy: The accuracy with which a user can return to a position whose coordinates have been measured at a previous time with the same navigation system.
- C. Relative Accuracy: The accuracy with which a user can measure position relative to that of another user of the same navigation system at the same time. This may be expressed also as a function of the distance between the two users. Relative accuracy may also refer to the accuracy with which a user can measure position relative to his own position in the recent past. For example, the present position of a craft whose desired track forms a specific geometric pattern in search operations or hydrographic survey, will be measured generally with respect to a previously determined datum.

2.3 AVAILABILITY

The availability of a navigation system is the percentage of time that the services of the system are usable by the navigator. Availability is an indication of the ability of the system to provide usable service within the specified coverage area. Signal availability is the percentage of time that navigational signals transmitted from external sources are available for use. It is a function of both the physical characteristics of the environment and the technical capabilities of the transmitter facilities. Formally, availability is the ratio of the mean-time-between-failures (MTBF) to the sum of the MTBF and the mean-time-to-repair (MTTR).

2.4 COVERAGE

The coverage provided by a radionavigation system is that surface area or space volume in which the signals are adequate to permit the navigator to determine position to a specified level of accuracy. Coverage is influenced by system geometry, signal power levels, receiver sensitivity, atmospheric noise conditions, and other factors which affect signal availability.

2.5 RELIABILITY

The reliability of a navigation system is a function of the frequency with which failures occur within the system. It is the probability that a system will perform its function within defined performance limits for a specified period of time under given operating conditions. Formally, reliability is one minus the probability of system failure.

2.6 FIX RATE

The fix rate is defined as the number of independent position fixes or data points available from the system per unit time.

2.7 FIX DIMENSIONS

This characteristic defines whether the navigation system provides a linear, one-dimensional line-of-position, or a two or three-dimensional position fix. The ability of the system to derive a fourth-dimension, i.e., time, from the navigational signals is also included.

2.8 SYSTEM CAPACITY

System capacity is the number of users a system can accommodate simultaneously.

2.9 AMBIGUITY

Ambiguity exists when the navigation system identifies two or more possible positions of the vehicle, with the same set of measurements, with no indication of which is the most nearly correct position. The potential for system ambiguities should be identified along with provision for users to identify and/or resolve them.

VOLUME III

CHAPTER 3

RADIONAVIGATION SYSTEM DESCRIPTIONS

3.0 SYSTEM DESCRIPTIONS

This section describes the characteristics of those individual radionavigation systems currently in use or under development. These systems are described in terms of the parameters defined in the previous section (2.0-2.9). All of the systems used for civil navigation are discussed. The systems which are used exclusively to meet the special applications of DOD are discussed in a classified supplement to this Plan.

3.1 LORAN-A

LORAN-A was developed during World War II to provide a long-range radionavigational capability. It was adopted by many civil maritime, and civil aviation users for navigation and position location.

3.1.1 Signal Characteristics

LORAN-A is a pulsed hyperbolic system operating in the 1700 to 2000 kHz band. The system is based on measurement of the difference in time of arrival of RF pulses radiated by a pair of synchronized transmitters which are separated by several hundred miles. Time-difference (TD) measurements are accomplished by using a specialized receiver to compare the leading edges of the envelopes of the received pulses. The difference in time is shown as a line of position (LOP) on a LORAN-A chart or derived from using LORAN tables. The TD measurements from two station pairs yields two LOPs. Their intersection defines a position fix. The characteristics of LORAN-A are summarized in Table III-3.1.

3.1.2 Accuracy

Accuracy of a LORAN-A fix varies with the location of the user in the service area, the relative geometry of the transmitting station pairs, and propagation conditions which vary with the time of day. Absolute or predictable accuracy varies from 1 to 2 NM (2 drms) using the ground wave, and 6 to 7 NM when using the sky wave at extended range. Repeatable accuracy is a function of the stability of the signal control system, the allowable tolerance on timing, and the variability in propagation conditions. LORAN-A has demonstrated repeatable accuracy ranging from .05 to 1.0 NM (90 to 1852m) 2 drms. Relative accuracy of LORAN-A is about the same as its repeatable accuracy but is greatly dependent upon the relative performance of LORAN-A receivers and operator skills.

System	Accuracy (95%)			Fix Rate	Coverage	Availability	Reliability	Ambiguity Resolution
	Predictable	Repeatable	Relative					
LORAN-C	0.25NM (worst case) for 1:3 SNR (460 m)	60-300 ft. (18-90 m)	60-300 ft. (18-90 m)	25 Fixes/ Second	U.S. Coastal Areas, Continental U.S., Selected Overseas Areas	99+%	(1)	Yes, Easily Resolved
LORAN-A	1-2NM (3.7-7.4km)	300-6000 ft. (90-1800 m)	300-6000 ft. (90-1800 m)	25 Fixes/ Second	U.S. Coastal Confluence, Bahamas	99%	(1)	Yes, Easily Resolved
OMEGA	2-4NM (goal) (3.7-7.4km)	2-4NM (3.7-7.4km)	1-2NM (1.85-3.7km)	1 Fix/ 10 Seconds	Near Global (over 90%)	99%	(1)	Requires Knowledge of Approx. Position

(1) depends on mission time

NOTE: Each system has unlimited capacity in terms of potential user populations, and all provide two-dimensional fixes.

TABLE III-3.1 System Characteristics (Signal-in-Space)

3.1.3 Availability

LORAN-A has demonstrated availability in excess of 99%.

3.1.4 Coverage

Coverage of the system is dependent upon the station power and propagation conditions. The groundwave range varies from 600-800 NM. Skywave range extends up to 1500 NM at night. The U.S. coverage of the LORAN-A System is shown in Figure III-3.1. Overseas LORAN-A stations, except those serving the Bahamas, ceased operation as of December 31, 1977. Domestic LORAN-A chains operated by the Federal Government and the Bahamas LORAN-A chain (which contributes to the coverage of southeastern U.S. waters) will be discontinued on a regional basis following an overlap of LORAN-A and LORAN-C service in the coastal zone.

Planned termination dates of U.S.-operated chains are given in Table III-3.2.

Table III-3.2

U.S. OPERATED LORAN-A CHAINS

Domestic

<u>Chain</u>	<u>Termination</u>
Aleutian Islands	July 1, 1979
Gulf of Alaska	December 31, 1979
Hawaiian Islands	July 1, 1979
West Coast	December 31, 1979
Bahamas	December 31, 1980
East Coast	December 31, 1980
Gulf of Mexico	December 31, 1980.

FIGURE III-3.1 U.S. LORAN-A Coverage

The primary users of LORAN-A are civil and military air and marine craft in transit out to the limit of groundwave coverage; beyond this range the skywave is used when available. Those vehicles interested in returning to the same location or traversing the same path, such as fishing vessels, utilize LORAN-A in the repeatable mode. LORAN-A has been used extensively in civil intercontinental air carrier operations for transoceanic flights, and is one of the systems certified by the FAA to bound the error of self-contained systems.

3.1.5 Reliability

There are no accurate reliability figures for the LORAN-A system because the subject is dependent upon the user's equipment and his operations. In general, reliability is high over any given twelve-hour period and users have expressed satisfaction with the past high availability of the systems.

3.1.6 Fix Rate

The fix rate of LORAN-A is dependent upon the pulse-repetition interval of the signal. LORAN-A will provide no less than 25 independent fixes per second at the shortest pulse-repetition interval.

3.1.7 Fix Dimension

LORAN-A will provide one line-of-position (LOP) per rate tracked. Two or more LOPs will provide a two-dimensional fix.

3.1.8 Capacity

The capacity of LORAN-A is unlimited.

3.1.9 Ambiguity

Because the LOPs are hyperbolic, it is theoretically possible for LOP's to cross at more than one place. However, this ambiguity is widely separated and easily recognized.

3.2 LORAN-C

LORAN-C was developed to provide DOD with a radionavigation capability having longer range and much greater accuracy than LORAN-A. It was subsequently selected as the U.S. Government-provided radionavigation system for civil marine use in the U.S. coastal areas.

3.2.1 Signal Characteristics

LORAN-C is a pulsed, hyperbolic system, operating in the 90-110 kHz frequency band. The system is based upon measurement of the difference in time of arrival of pulses of RF energy radiated by a chain of synchronized transmitters which are separated by hundreds of miles. The measurements of time-difference (TD) are made by a receiver which achieves improved accuracy over LORAN-A by comparing a zero crossing of a specified RF cycle within the pulses transmitted

by master and secondary stations within a chain. Making this comparison early in the pulse assures that the measurement is made before the arrival of the corresponding skywaves. Precise control over the pulse shape ensures that the proper comparison point can be identified by the receiver. To prevent sky waves from affecting TD measurements, the phase of the 100 kHz carrier of each pulse is changed in a predetermined pattern. Envelope matching of the signals is also possible but cannot provide the advantage of cycle comparison in obtaining the full system accuracy. The characteristics of LORAN-C are summarized in Table III-3.1.

3.2.2 Accuracy

Within the groundwave range, LORAN-C will provide the user, who employs an adequate receiver, with predictable accuracy of 0.25 NM (2 drms) or better. The repeatable and relative accuracy of LORAN-C is usually between 18 to 90 meters. All accuracy is dependent upon the Geometric Dilution of Precision (GDOP) factors at the user's location within the coverage area.

The LORAN-C groundwave is used primarily for navigation. Skywave navigation is feasible, but with some loss in accuracy. Both groundwaves and skywaves may be used for measuring time and time interval. Although it is designed for use, and normally operated in the hyperbolic mode, LORAN-C can be used to obtain accurate fixes by determining the range to individual stations. This is accomplished by a comparison of the received signal phase to a known time reference to determine propagation time and, therefore, range from the stations. This is referred to as the range-range (rho-rho) mode. It can be used in situations where the user is within reception range of individual stations, but beyond the hyperbolic coverage area. The rho-rho method of using LORAN-C requires that the user have a very precise and stable time reference. The high cost of equipment of this type limits the use of this mode.

The inherent accuracy of the LORAN-C system makes it a suitable candidate for many land radiolocation applications. The purely numeric Time Difference (TD's) readings (no names, words, or narratives) are easy and efficient to both store and retrieve in automated form. Since the data is purely numeric, there can be none of the ambiguity that results from attempting to retrieve narrative descriptors from traffic accident reports or highway inventory data. While the 100 kHz signal is affected to some extent by soil conductivity and terrain, it can be received in mountainous areas where VHF and UHF systems are unusable; however, some distortion of the hyperbolic grid has been noted. Propagation anomalies may be encountered in urban areas where the proximity of man-made structures affects the signal. The existence of these anomalies is predictable and can be compensated for, usually by surveying the area. The long range of the LORAN-C system makes it particularly desirable for application to remote areas, or where the user population is too low to justify the cost of a large number of short-range facilities.

By monitoring LORAN-C signals at a fixed site, the receiver TD can be compared with a computed TD for the known location of the site. A correction for the area can then be broadcast to users. This technique (called Differential LORAN-C), whereby real-time corrections are applied to LORAN-C TD readings, provides improved accuracy. This method shows promise of providing the higher precision needed for marine navigation in harbor approaches and inland waterways. Another technique involves installing short-baseline, low-power chains to serve specific restricted areas. Such a chain is being tested and evaluated in the St. Marys River in the Great Lakes. In other locations a low-power transmitter can serve as an additional secondary station to improve the grid geometry and signal strength in a local area.

LORAN-C receivers are available at a relatively low cost and achieve the 0.25 NM (2 drms) accuracy that LORAN-C is capable of providing. A LORAN-C receiver which will be useful to the limits of the specified coverage areas for the U.S. coastal zone has the following characteristics:

- o It acquires the LORAN-C signals automatically, without the use of an oscilloscope.
- o It accomplishes cycle matching on all pulses to take advantage of the maximum accuracy of the system.
- o It automatically tracks the signals once they have been acquired.
- o It displays at least two time-difference readings, with resolution of at least 0.1 microsecond, to provide a two-line of position fix.

3.2.3 Availability

LORAN-C transmitting requirement is very reliable. Redundant systems are used to reduce system downtime. Exclusive of infrequent periods of scheduled off-air for tower maintenance, LORAN-C availability is greater than 99% per year.

3.2.4 Coverage

Until recently, there had been three LORAN-C chains providing coverage for the U.S. and Canadian coastal waters. An East Coast Chain comprised of five stations has provided groundwave coverage for most of the East Coast from Nova Scotia to Florida, a very small part of the coastal waters of the Gulf of Mexico, and a portion of the Great Lakes. A North Pacific Chain, comprised of four stations, has provided coverage for the Bering Sea, Aleutian Islands, and adjacent North Pacific and Alaska waters. A Hawaiian Chain, comprised of three stations, has provided coverage for the waters in the vicinity of the Hawaiian Islands north of Johnston Island between Midway and Kauai.

Expansion of the LORAN-C system, to meet the requirements for the U.S. coastal waters of the conterminous 48 states and southern Alaska, will be complete in late 1979. Stations have been built to provide service to the U.S. West Coast, the Gulf of Alaska, southeastern Alaska and the Gulf of Mexico. The Government of Canada has constructed a LORAN-C station in British Columbia to operate in conjunction with U.S. stations in Washington and Alaska. Thus, coastal LORAN-C service will be complete from the U.S.-Mexican border northward through the Gulf of Alaska and the Aleutians and into the Bering Sea. Required service to the East Coast and Great Lakes will be provided by reconfiguring four stations of the existing East Coast Chain and construction of five new stations to form three new chains. The new LORAN-C service for the Great Lakes is planned to be operational by mid-1980 when the final station is complete. The coastal LORAN-C service will also provide overland coverage to about two-thirds of the land area of the conterminous 48 states. Planned coverage of the reconfigured system is shown in Figure III-3.2.

Plans are under consideration for further expansion of the LORAN-C system to provide coverage for the remaining land areas of the conterminous 48 states. The radionavigation requirements for Hawaii, Puerto Rico, and the U.S. Virgin Islands and the north slope of Alaska are under study.

3.2.5 Reliability

The accurate reliability figures for LORAN-C were not available at the time this Plan was written. In general, the MTBF of the system will be used to categorize the reliability.

3.2.6 Fix Rate

The fix rate available from LORAN-C is not less than 10 fixes per second.

3.2.7 Fix Dimension

LORAN-C will furnish two or more LOPs to provide a two-dimensional fix.

3.2.8 Capacity

An unlimited number of receivers may be used on LORAN-C simultaneously.

3.2.9 Ambiguity

As with all hyperbolic systems, theoretically, the LOPs may cross at more than one position on the earth. However, because of the design of the coverage area, the ambiguous fix is at a great distance from the desired fix and is easily resolved.

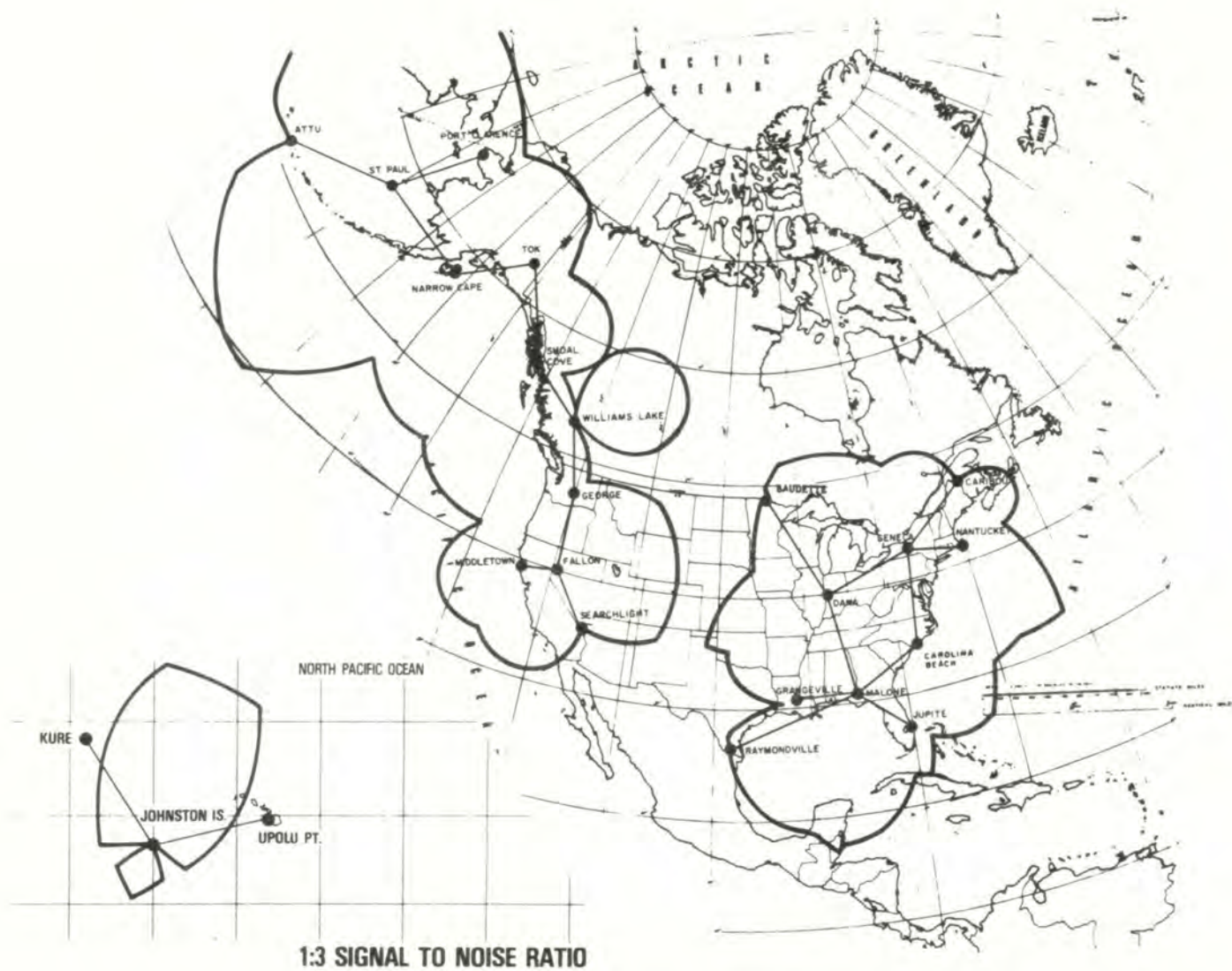


FIGURE III-3.2 Planned U.S. LORAN-C Coverage

3.3 VOR, VOR/DME, TACAN

The three systems that provide the basic guidance for en route air navigation in the U.S. are VHF Omnidirectional Range (VOR), Distance Measuring Equipment (DME), and Tactical Air Navigation (TACAN). Information provided to the aircraft pilot by VOR is the azimuth relative to the VOR ground station. DME provides a measurement of distance from the aircraft to the DME ground station. In most cases, VOR and DME are collocated as a VOR/DME facility. TACAN provides both azimuth and distance information and is used primarily by military aircraft. When TACAN is collocated with VOR, it is a VORTAC facility. DME and the distance measuring function of TACAN are the same.

3.3.1 VOR Signal Characteristics (VHF Omni-Range)

The VOR transmits two 30 HERTZ (Hz) modulations with a relative electrical phase angle equal to the azimuth angle of the receiving aircraft. A cardioid field pattern is produced in the horizontal plain and rotates at 30 HERTZ. A non-directional (circular) 30 Hz pattern is also transmitted during the same phase in all directions and is called the reference phase signal. The variable phase, figure 8, signal changes phase in direct relationship to azimuth. The reference phase is frequency modulated while the variable phase is amplitude modulated. The receiver detects these two signals and computes the azimuth from the relative phase difference. For difficult siting situations, a system using the Doppler effect was developed which uses 50 instead of 4 antennas for the variable phase. The same avionics works with either type ground station. There are about 30 such stations out of approximately 1000 presently in operation. An additional 30 are being developed for additional difficult sites. VOR frequencies are assigned in the 108 to 118 megahertz frequency band and are separated by 100 KHz. The capability for 50 kHz separation has been developed but not yet implemented. The signal characteristics of VOR are summarized in Table III-3.3.

A. Accuracy (2 sigma)

1. Predictable Errors

The ground station errors are approximately ± 1.4 degrees. The addition of course selection, receiver and flight technical errors, when combined using root-sum-squared (RSS) techniques, is calculated to be ± 4.5 degrees.

2. Relative Errors

Although some course bending could influence position readings between aircraft, the major relative error consists of the course selection, receiver and flight technical components. When combined using RSS techniques, the value is approximately ± 4.3 degrees. The VOR ground station relative error is ± 0.35 degrees.

System	Description	Accuracy			Availability	Coverage	Reliability	Fix Rate	Fix Dimension	Capacity	Ambiguity Potential
		Predictable	Repeatable	Relative							
VOR	VHF Signal Providing Omnidirectional Azimuthal Information (Aviation Use)	90m ($\pm 1.4^\circ$) ^{1/}	23-292m ($\pm 0.35^\circ$) ^{2/}	23-292m ($\pm 0.35^\circ$) ^{2/}	Approaches 100% Warning if Not Providing Published Service	Line of Sight (Present Air Routes)	Approaches 100% Warning if Not Providing Published Service	Continuous	Heading in Degrees or Angle Off Course	Unlimited	None
TACAN (Azimuth Only)	UHF Signal Providing Omnidirectional Azimuthal Information (Aviation Use)	63m ($\pm 1.0^\circ$) ^{3/}	63m ($\pm 1.0^\circ$) ^{3/}	63m ($\pm 1.0^\circ$) ^{3/}	"	"	"	"	"	Approx 200 users per site	Slight
DME (Same for TACAN and VOR-DME)	UHF Signal Providing Ranging Information (Aviation Use)	185m (± 0.1 nm)	185m (± 0.1 nm)	185m (± 0.1 nm)	"	"	"	"	N.M. (Slant Range)	Approx. 100 Users per Site for Full Service	None

^{1/} The flight check of published procedures for the VOR signal is $\pm 1.4^\circ$. The ground monitor turns the system off if the signal exceeds $\pm 1.0^\circ$. The cross track error used in the chart is for $\pm 1.4^\circ$ at 2nm from the VOR site. However, some uses of VOR are overhead and or 1/2nm from the VOR.

^{2/} Test data shows that 99.94% of the time the error is less than $\pm 0.35^\circ$. These values are for $\pm 0.35^\circ$ at 2nm from the VOR.

^{3/} The TACAN specification is $\pm 1.0^\circ$ and the monitor is set at $\pm 1.0^\circ$. The cross track errors are for $\pm 1.0^\circ$ at 2nm from the TACAN.

TABLE III-3.3 Radionavigation Systems Characteristics (Signal-in-Space)

3. Repeatable Errors

The major error components of the ground system and receiver will not vary appreciably in the short term. Therefore, the repeatable error will consist mainly of the flight technical errors (the pilots' ability to fly the system) which is ± 2.3 degrees.

B. Availability

Recognizing the fact that the VOR equipments are redundant and that the facilities are overlapped by adjacent stations (Extended Service Volume), the availability is considered to approach 100%.

C. Coverage

The VOR has line-of-sight limitations which could limit ground coverage to 30 miles or less. At altitudes above 5000 feet the range is approximately 100 NM and above 20,000 feet the range will approach 200 NM. These stations radiate approximately 200 watts. Terminal VOR stations are rated at approximately 50 watts and are only intended for use within the terminal areas.

D. Reliability

Due to advanced solid state construction and the use of remote maintenance monitoring techniques, the reliability of VOR is assumed to approach 100%. In addition, the station monitors will automatically shutdown an out-of-tolerance station and the receivers will give an immediate and positive indication of loss of signal.

E. Fix Rate

This system allows a continuous update of deviation from a selected course. Initialization is less than one minute after turn-on and will vary as to receiver design.

F. Fix Dimension

The system shows a bearing to a VOR station and a deviation from a selected course, in degrees.

G. Capacity

The capacity of a VOR station is unlimited.

H. Ambiguity

There is no ambiguity possible for a VOR station.

3.3.2 DME Signal Characteristics (Distance-Measuring Equipment)

The interrogator in the aircraft generates a pulsed signal (interrogation) which, when of the correct frequency and pulse spacings, are accepted by the transponder. In turn, the transponder generates pulsed signals (replies) which are sent back and accepted by the interrogator's tracking circuitry. Distance is then computed by measuring the total round trip time of the interrogation and its reply. The operation of DME is thus accomplished by paired pulse signals and the recognition of desired pulse spacings accomplished by the use of a decoder. The transponder must reply to any one of many interrogations frequencies. The interrogator must measure elapsed time between interrogations and reply pulse pairs and translate this to distance. This must be accomplished for only replies to its interrogation. All signals are vertically polarized. These systems are assigned in the 960 to 1215 megahertz frequency band with a separation of 1 megahertz. The capability to use 50 kHz separation has been developed but not implemented. The signal characteristics of DME are summarized in Table III-3.3.

A. Accuracy (2 sigma)

1. Predictable Errors

The ground station errors are less than ± 0.1 NM. The overall system error (airborne and ground RSS) is not greater than ± 0.5 NM or 3% of the distance, whichever is greater.

2. Relative Errors

Although some errors could be introduced by reflections, the major relative error emanates from receiver and flight technical error.

3. Repeatable Error

Major error components of the ground system and receiver will not vary appreciably in the short term.

B. Availability

The availability of DME is considered to approach 100%, with positive indication when the system is out of tolerance.

C. Coverage

The DME has a line-of-sight limitation, which limits ground coverage to 30 NM or less. At altitudes above 5,000 feet, the range will approach 100 NM. These stations radiate at 1000 watts. Terminal DMEs radiate 100 watts and are only intended for use in terminal areas.

D. Reliability

With the use of solid state components and remote maintenance monitoring techniques, the reliability of the DME approaches 100%. The monitors automatically shutdown an out-of-tolerance station.

E. Fix Rate

The system essentially gives a continuous update of distance to the facility. Actual update rate varies with the design of airborne equipment and system loading.

F. Fix Dimension

The system shows distance to the DME station in NM.

G. Capacity

110 interrogators are considered reasonable for present handling. Future traffic capacity could be increased when necessary through reduced airborne interrogation rates.

H. Ambiguity

There is no ambiguity in the DME system.

3.3.3 TACAN Signal Characteristics (Tactical Air Navigation)

The TACAN system is a combination of omni-bearing and distance-measuring functions. The important feature of this ground system is the rotating directional radiation pattern produced in an horizontal plane. The azimuth portion consists of coarse azimuth (15 Hz) and fine azimuth (135 Hz) elements. The rotation of the patterns at 15 Hz results in a modulation of the RF carrier with a composite 15 Hz sine wave to the aircraft. Reference signals in the form of pulse trains are added to the radiated signal to provide electrical phase. The 135 Hz sine wave signal provides an additional accuracy feature to the TACAN system, thereby reducing bearing error. Bearing is obtained by comparing the 15 and 135 Hz sine waves with the reference groups. TACAN operates in the 960-1215 megahertz band with frequency assignments separated by 1 megahertz. The signal characteristics of TACAN are summarized in Table III-3.3.

A. Accuracy (2 Sigma)

1. Predictable Error

The ground station errors are less than +1.0 degree for azimuth for the 135 Hz band and +4.5 degrees for the 15 Hz band and +0.1 NM distance.

2. Relative Errors

The major relative errors would emit from course selection, receiver and flight technical error.

3. Repeatable Errors

Major error components of the ground station and receiver will not vary greatly in the short term. The repeatable error will consist mainly of the flight technical error -- the pilot's ability to fly the system.

B. Availability

The availability of TACAN is considered to approach 100%.

C. Coverage

The TACAN has a line-of-sight limitation which limits ground coverage to 30 NM or less. At altitudes of 5,000 feet the range will approach 100 NM; above 18,000 feet, the range approaches 130 NM. The station output power is 5 KW.

D. Reliability

With the use of solid state electronics and remote maintenance monitoring techniques, the reliability of the TACAN system approaches 100%. Monitors automatically shut down an out-of-tolerance station.

E. Fix Rate

This system provides a continuous update of the deviation from a selected course. Initialization is less than one minute after turn on. Actual update rate varies with the design of airborne equipment and system loading.

F. Fix Dimension

The system shows bearing to a TACAN station and deviation in degrees and distance to the TACAN station in NM.

G. Capacity

For distance information, 110 interrogators are considered reasonable for present traffic handling. Future traffic handling could be increased when necessary through reduced airborne interrogation rates.

H. Ambiguity

There is no ambiguity in the TACAN range information. There is a slight probability of azimuth ambiguity.

3.4 OMEGA

The OMEGA system was proposed initially to meet a DOD need for worldwide general en route navigation. The system is comprised at present of seven of eight planned CW transmitting stations situated throughout the world and one temporary station located in Trinidad. Nearly worldwide position coverage will be attained when the eighth permanent station in Australia becomes operational in 1980.

3.4.1 Signal Characteristics

OMEGA utilizes CW phase comparison of skywaves from pairs of stations. The stations transmit time shared signals on four frequencies: 10.2 kHz, 11-1/3 kHz, 13.6 kHz, and 11.05 kHz. In addition to these common frequencies, each station transmits a unique frequency to aid station identification and to enhance receiver performance. The signal characteristics of OMEGA are summarized on Table III-3.1.

3.4.2 Accuracy

The inherent accuracy of the OMEGA system is limited by the accuracy of the propagation corrections that must be applied to the individual receiver readings. The corrections may be obtained in the form of predictions from tables or automatically in computerized receivers. The system has as a design goal a predictable accuracy of 2 to 4 NM (2 drms). This depends on location, station pairs used, time of day, and validity of the propagation corrections. However, when the system is complete, it is expected that there will be some marginal coverage and degraded accuracy in certain areas of the world.

Propagation correction tables are based on theory and modified to fit monitor data taken over long periods for localized areas. An extensive monitoring program is being undertaken. The monitor network will be used to verify the propagation model used to predict the corrections and the system accuracy in the area of the network stations. A number of permanent monitors will be maintained to update the model on a long-term basis. The system is currently usable and provides coverage over more than 90 percent of the earth and nearly all of the Northern Hemisphere. The specific accuracy and coverage depends on the type of equipment used, level of operator training, time of day, and related factors. In many cases, accuracies of 2 NM (2 drms) day and 4 NM (2 drms) night are being achieved or exceeded. Although the system is usable, a continuing program of monitoring and validating OMEGA signals must be completed before the system can be considered fully operational. This validation program, which will help define system capabilities and limitations, will be carried out on a regional basis. As each region is validated, it will be declared operational. Full worldwide validation depends on the eighth and final permanent station being completed and its signals evaluated.

3.4.3 Availability

Exclusive of infrequent periods of scheduled off-air time for tower maintenance, OMEGA availability is greater than 99% per year for each station and 95% for three stations. An evaluation of maintenance during on-air operation is ongoing. If successful, availability can be increased accordingly. System availability has been greater than 97% with scheduled off-air time included.

3.4.4 Coverage

When the OMEGA system is fully implemented, it will provide air and maritime users with a nearly worldwide position verification system. It will provide airborne self-contained systems with the means to bound accumulated dead-reckoning (DR) error. Preliminary test data obtained in the operational environment have indicated that performance will satisfy the requirements established for oceanic airspace. However, the operational significance of lane slips, solar flares, and polar cap absorption must be considered. When fully qualified, the OMEGA system should satisfy the long-standing requirement for an externally-referenced radio-navigation system for aircraft in high density oceanic airspace.

Federal Aviation Regulations require the use of an independent position system with Doppler systems in order to limit potential navigational errors, on flight legs of 1000 NM or greater. It is doubtful that OMEGA will be acceptable as the primary navigational aid in the domestic air traffic system because of the possible lack of usable signals in the North Central U.S. This situation is under investigation.

3.4.5 Reliability

Reliability figures for OMEGA were not available at the time this Plan was written. In general, the mean-time-between failures of the system will be used to categorize the reliability. It is expected to be greater than 99%.

3.4.6 Fix Rate

The OMEGA system provides independent positional fixes once every ten seconds.

3.4.7 Fix Dimension

OMEGA will furnish two or more LOPs to provide a two-dimensional fix.

3.4.8 Capacity

An unlimited number of receivers may be used simultaneously

3.4.9 Ambiguity

In this CW system, ambiguous LOP's occur as there is no means to identify particular points of constant phase difference which recur periodically throughout the coverage area. The area between lines of zero phase difference are termed "lanes." Single-frequency receivers use the 10.2 kHz signals whose lane width is about eight miles on the baseline between stations. Multiple-frequency receivers extend the lane width, but these are more expensive than single-frequency receivers. Because of the lane ambiguity, receivers must be preset to a known location. Once set to a known location, the OMEGA receiver counts the number of lanes it crosses in the course of a voyage. This lane count is subject to errors which may be introduced by an interruption of power to the receiver, changes in propagation conditions near local sunset and sunrise, and other factors. To use

OMEGA effectively for navigation, it is essential that a DR plot be maintained carefully, and that the DR and OMEGA positions be compared periodically so that "jumps" in the OMEGA lane count can be detected and corrected. The accuracy of an OMEGA phase-difference measurement is independent of the elapsed time or distance since the last update. Unless the OMEGA position is verified occasionally by comparison to a fix obtained with another navigation system or by periodic comparison to a carefully-maintained DR plot, the chance of an error in the OMEGA lane count increases with time and distance.

3.5 RADIOBEACONS

Radiobeacons are nondirectional radio transmitting stations which operate in the low frequency (LF) and medium frequency (MF) bands to provide groundwave signals to a receiver. A radio direction finder (RDF) is used to measure the relative bearing of the transmitter with respect to the heading of an aircraft or vessel.

Presently, there are approximately 1500 LF and MF nondirectional beacons operated for the benefit of aviation users. These are distributed about as follows: FAA 600, non-Federal 700, and military 200. No change in the status of these facilities is contemplated earlier than 1985 and probably not until 2000.

There are approximately 200 Coast Guard-operated marine radiobeacons. Operation of these systems will be continued through the 1990's. The system is being modernized, expanded slightly and reconfigured to provide better service in response to the increasing demand. This effort includes establishing 37 new stations, relocation of some others, changes in type of operation of selected beacons, and changes in frequency. These changes will improve service by providing more beacons, improving signal availability, and providing service in many areas where coverage does not exist. The changes in frequency will result in more efficient use of the RF spectrum and will allow for additional beacons in some areas if needed.

3.5.1 Signal Characteristics

Aeronautical Nondirectional Beacons (NDB) operate in the 200-415 kHz band. Marine radiobeacons operate in the 285-325 kHz band. The transmissions include a coded continuous-wave (CCW) or modulated continuous-wave (MCW) signal to identify the station. Two CW carriers are spaced 1000 Hz apart, one of which is keyed intermittently to produce the code characters. Some of the longer-range marine radiobeacons operate on the same frequency and are time sequenced to prevent mutual interference.

3.5.2 Accuracy

Positional accuracy derived from the bearing information is a function of geometry of the LOPs, the accuracy of compass heading, measurement accuracy, distance from the transmitter, stability of the signal, nature of the terrain between beacon and craft, and noise. In practice, bearing accuracy is of the order of ± 3 degrees. Achievement of this accuracy requires that the RDF be calibrated before it is used for navigation by comparing radio bearings to accurate bearings obtained visually on a transmitting antenna that is within visual range. Since most direction-finder receivers will tune to a number of radio frequency bands, transmissions from

sources of known location, such as AM broadcast stations, are also used to obtain bearings, generally with less accuracy than obtained from radiobeacon stations because these signals are not calibrated. For FAA flight inspection, NDB system accuracy is stated in terms of permissible needle swing: ± 5 degrees on approaches and ± 10 degrees in the en route area.

3.5.3 Availability

Availability of marine and aeronautical radiobeacons is in excess of 99%.

3.5.4 Coverage

The coverage of marine radiobeacons is shown in Figure III-3.3. Extensive coverage of NDBs is provided by 1500 stations, of which the FAA operates 600.

3.5.5 Reliability

Reliability is in excess of 99%.

3.5.6 Fix Rate

The fix rate is a function of whether the beacon is continuous or sequenced. In general, at least one line of position, or relative bearing, is provided continuously. If sequenced, fixing a position may require up to six minutes, depending on LOPs selected.

3.5.7 Fix Dimension

In general, one line of position is available from a single radiobeacon. If within range of two or more beacons, a two-dimensional fix may be obtained.

3.5.8 Capacity

An unlimited number of receivers may be used simultaneously.

3.5.9 Ambiguity

The only ambiguity which exists in the radiobeacon system is one of reciprocal bearing provided by some receiving equipment which does not employ a sense antenna to resolve direction.

3.6 AIRCRAFT LANDING SYSTEMS

At present, the Instrument Landing System (ILS) is the primary worldwide, ICAO-approved, precision landing system. This system is presently adequate, but has limitations in siting, frequency allocation, cost, and performance. An alternate system, scanning beam Microwave Landing System (MLS) has been developed and approved by the ICAO. This new system is expected to be implemented and eventually replace the ILS.



FIGURE III-3.3 Radiobeacon Coverage

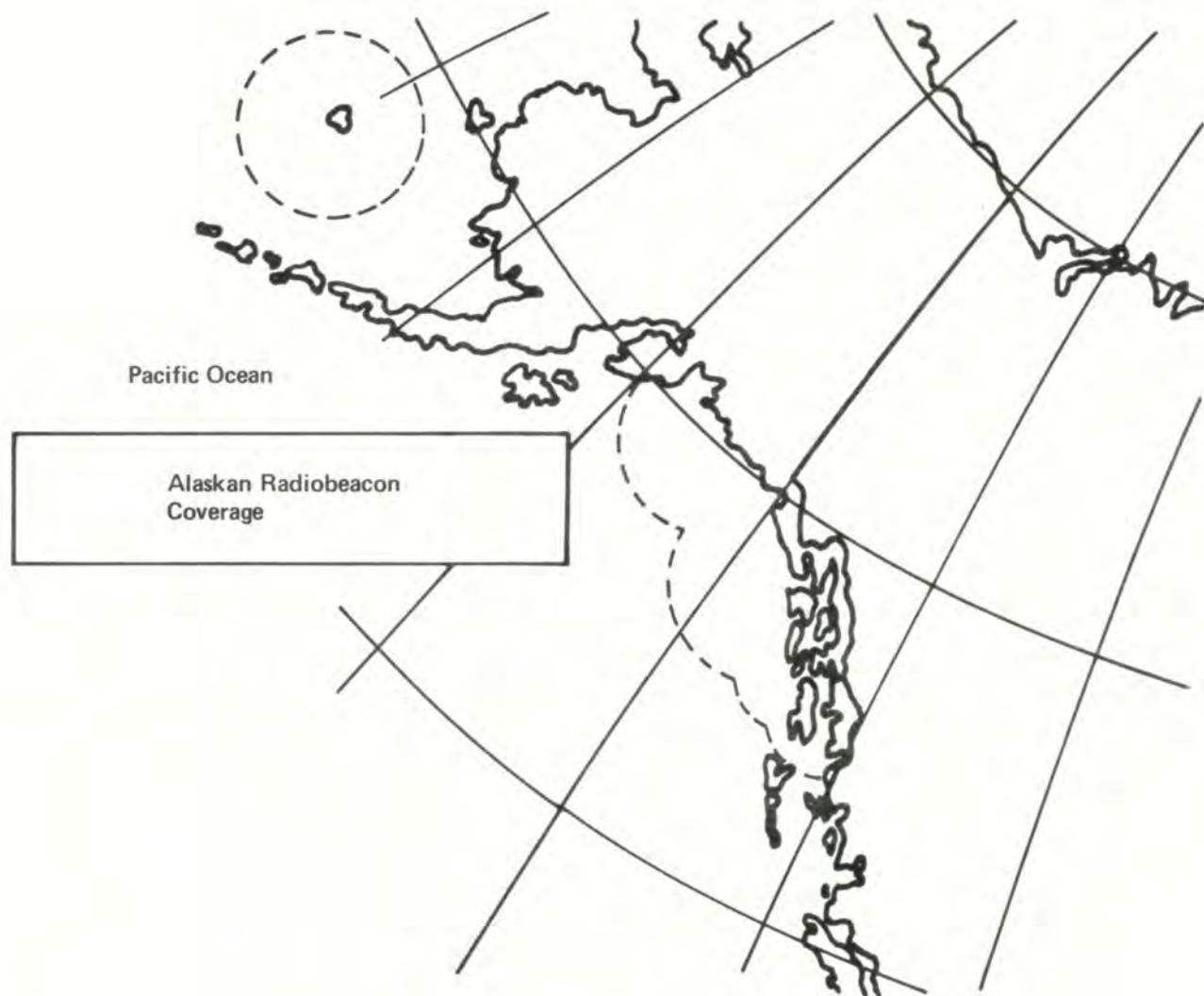


FIGURE III-3.3 (Continued)



FIGURE III-3.3 (Continued)

3.6.1 Instrument Landing System

ILS is a precision approach system normally consisting of a localizer facility, a glide slope facility, and two or three VHF marker beacons. It provides vertical and horizontal navigational (guidance) information during the approach to landing at an airport runway.

A. Signal Characteristics

The localizer facility and antenna are typically located 1000 feet beyond the stop end of the runway and provides a VHF (108-112 MHz) signal. The glide slope facility is located approximately 1000 feet from the approach end of the runway and provides a UHF (328.6-335.4 MHz) signal. Marker Beacons are located along the extension of the runway centerline to indicate to the pilot decision height points or distance to the runway threshold, they emit a 75 MHz signal. The signal characteristics of ILS are summarized in Table III-3.4.

B. Accuracy

For typical air carrier operations at a 10,000 foot runway, the course alignment (localizer) at threshold is maintained within ± 25 feet. Course bends during the final segment of the approach do not exceed ± 0.06 degrees (2 sigma). Glide slope course alignment is maintained within ± 7.0 feet at 100 feet (2 sigma) elevation and course bends during the final segment of the approach do not exceed ± 0.07 degrees (2 sigma).

C. Availability

While the availability of existing installations has been adequate, many are vacuum tube installations and are being replaced with solid state equipment to further improve availability

D. Coverage

As of March 31, 1979, there were 581 ILS installations operated by the FAA, plus 10 approved facilities operated by other agencies. Approximately 160 new ILS facilities will be installed through 1981.

Coverage for individual systems is as follows:

Localizer:	$\pm 2^{\circ}$ centered about runway centerline
Glide Slope:	Nominally 3° above the horizontal
Marker Beacons:	$\pm 40^{\circ}$ (approximately) on minor axis (along approach path)
	$\pm 85^{\circ}$ (approximately) on major axis

E. Reliability

ILS reliability, which is adequate, will be improved as the vacuum tube equipment is replaced by newer solid state units. As a related factor, however, terrain and other factors may impose limitations upon the use of the ILS signal. Special account must be taken of terrain factors and dynamic factors such as taxiing aircraft which can cause multipath signal transmissions. In some cases, to resolve ILS siting problems, use has been made of localizers with wide aperture antennas and two-frequency systems. In the case of the glide slope, use has been made of wide aperture, two frequency-image arrays and single-frequency broadside arrays to provide service at difficult sites.

System		Accuracy* 2 Sigma meters			Availability	Coverage	Reliability	Fix Rate	Fix Dimensions	System Capacity	Ambiguity
		Predictable	Repeatable	Relative							
ILS	Cat I	N/A	9.1	9.1	Approaches 100% with Positive Indication when the System is out of Tolerance	From Center of Localizer Antenna $\pm 10^{\circ}$ out to 35NM and $\pm 35^{\circ}$ out to 17NM	98.6% with Positive Indication when the System is out of Tolerance	Continuous	Heading and Deviation in Degrees	Limited Only by Aircraft Separation Requirements	None
	Cat II		4.6	4.6							
	Cat III		4.1	4.1							
MLS	Cat I	N/A	9.1	9.1	"	$\pm 60^{\circ}$ from Center Line of Runway out to 20NM in Both Direc- tions. Provisions for 360° out to 20NM	Approaches 100% with Positive Indication when the System is out of Tolerance	From 6.5 to 39 Fix/Sec Depending on Function	Heading and Deviation in Degrees. Range in NM	"	None
	Cat II		4.6	4.6							
	Cat III		4.1	4.1							

*Lateral accuracies at decision height

TABLE III-3.4 ILS/MLS System Characteristics (Signal-in-Space)

F. Fix Rate

The glide slope and localizer provide continuous fix information. Marker beacons which provide an audible and visual indication to the pilot are sited at specific points along the approach path as indicated in Table III-3.5.

G. Fix Dimension

ILS provides both vertical and horizontal guidance with glideslope and localizer signals. At periodic intervals (passing over marker beacons) distance to threshold is obtained.

H. Capacity

ILS has no capacity limitations except those imposed by aircraft separation requirements since aircraft must be in trail to use the system.

I. Ambiguity

Any potential ambiguities are resolved by imposing system limitations as described in Section 3.6.1-E.

3.6.2 Microwave Landing System

The Microwave Landing System (MLS) has been developed by DOT, DOD, and NASA to provide a common civil/military landing system to meet the full range of user operational requirements to the Year 2000 and beyond. It is intended as a replacement for the Instrument Landing System (ILS) used by both civil and military aircraft and the Ground Controlled Approach system used primarily by military operators. The signal is transmitted throughout a large volume of airspace, thereby permitting service to multiple aircraft, along multiple approach paths, throughout the approach, flare, touchdown, and rollout maneuvers. The system permits greater flexibility in air traffic procedures, enhancing safety, and permits curved and segmented approach paths for purposes of noise abatement. It allows reduced intervals between aircraft to increase runway acceptance rates, and facilitates short field operations for short and/or vertical takeoff and landing (STOL and VTOL) aircraft.

A. Signal Characteristics

The MLS transmits signals that enable airborne units to determine the precise azimuth angle, elevation angle, and range. The technique chosen for the angle function of the MLS is based upon Time-Referenced Scanning Beams (TRSB). All angle functions of MLS operate in the 5.00-5.25 GHz band. Ranging is provided by DME operating in the 0.96-1.215 GHz band. An option is included in the signal format to permit a special purpose system to operate in the 15.4-15.7 GHz band. The signal characteristics of MLS are summarized in Table III-3.4.

TABLE 3.5

AIRCRAFT MARKER BEACON

<u>Marker Designation</u>	<u>Distance to Threshold</u>	<u>Height (Ft. Per Sec.)</u>	<u>Audible Signal</u>	<u>Light Color</u>
Outer	4.5-4.7NM	Glide Slope Intercept	2 dashes	Purple
Middle	2000-6000 ft	200	1 dot-dash	Amber
Inner	1000 ft	100	6 dots	White

B. Accuracy (2 Sigma)

The azimuth accuracy is ± 13.5 feet at touchdown on a 14,000 foot runway. The elevation accuracy is ± 2.0 feet at runway threshold. The flare guidance accuracy is ± 2.0 feet throughout the touchdown zone and the DME accuracy is ± 100 feet for the precision mode and ± 1600 feet for the nonprecision mode.

C. Availability

Equipment redundancy, as well as remote maintenance monitoring techniques, should allow the availability of this system to approach 100%.

D. Coverage

MLS provides data over a wide volume, bounded by ± 60 degrees from runway centerline, 0 to 30 degrees elevation and up to at least 20 NM range from the threshold. The signal format also provides for 360° azimuth coverage, a feature not presently required, but one which might possibly be considered useful at some future time. Present plans are that 380 MLS facilities will be installed by 1986. By the Year 2000, approximately 1250 MLS facilities will be in place. There will be a simultaneous phase-out of ILS.

E. Reliability

The MLS signals are generally much less sensitive than ILS signals to the effects of snow, vegetation, terrain, structures, and taxiing aircraft. This allows the reliability of this system to approach 100%.

F. Fix Rate

Elevation angle is transmitted at 39 samples per second and azimuth angle at 13 samples per second. Usually the airborne receiver averages several data samples to provide fixes of 3 to 6 samples per second.

G. Fix Dimensions

This system provides signals in all three dimensions and can provide time if aircraft are suitably equipped.

H. Capacity

DME signals of this system are capacity limited, the system limits are approached when 110 aircraft are handled.

I. Ambiguity

No ambiguity is possible for the azimuth or elevation signals. Only a very small probability for ambiguity exists for the range signals and then only for multipath caused by moving reflectors.

3.7 NAVSTAR GPS

NAVSTAR GPS is a space-based radionavigation system being developed by the Department of Defense under Air Force management. The fully-deployed operational system is intended to provide highly accurate position and velocity information in three dimensions and precise time and time interval on a global basis continuously, to an unlimited number of properly-equipped users. It will be unaffected by weather and will provide a worldwide common grid reference system. The objective of the program is to provide very precise positional information for a wide spectrum of military missions. In addition, current policy calls for civil availability with a degradation in system accuracy required to protect U.S. national security interests. The characteristics of NAVSTAR GPS are summarized in Table III-3.6.

3.7.1 Signal Characteristics

The NAVSTAR GPS concept is predicated upon accurate and continuous knowledge of the spatial position of each satellite in the system with respect to time and distance from a transmitting satellite to the user. Each satellite transmits its ephemeris data. This is periodically updated by the master control station based upon data obtained from the monitors.

The user system automatically selects appropriate signals from each of the four satellites (selected from those in view with respect to optimum satellite-to-user geometry). It then solves the three time-of-arrival difference quantities to obtain distance between user and satellites. This information establishes the user position with respect to the satellite system. A time correction factor then relates the satellite system to earth coordinates. Each satellite will continuously transmit a composite signal at 1227.6 and 1575.42 MHz consisting of a precise navigational signal, a coarse/acquisition navigational signal, data such as satellite ephemeris, atmospheric propagation correction data and clock bias information. User segment equipment measures four independent pseudoranges and range-rates and translates these to three-dimensional position, velocity and system time.

System	Description	Accuracy ^{1/}			Avail.	Coverage	Rel.	Fix Rate	Fix Dim.	Capacity	Ambiguity Potential
		Pred.	Repeat.	Relative							
TRANSIT	Satellite Doppler	500m	50m	38m	99+% when Satellite is in View	Worldwide Non-Continuous	—	30 Min. at 80° lat. to 110 min. at Equator (Average)	2D	Unlimited	—
NAVSTAR GPS	Satellite, UHF Spread Spectrum Structured Navigation Signal	Horiz. 25m Vert. 30m	25m 30m	10m 8m	95%	Global Continuous	99+%	Essentially Continuous	3D+ Time and 3D Velocity	Unlimited	—

NOTE: Horizontal (2 drms) and vertical (2 sigma) accuracies are available to military and selected civil users. Accuracy available to other users is estimated at: 500m (2 drms) horizontal and 430m (2 sigma) vertical.

TABLE III-3.6 System Characteristics for Selected Radionavigation Systems

3.7.2 Accuracy

Accuracy of a NAVSTAR GPS fix varies with the capability of the user equipment and the user-to-satellite geometries.

- A. The most sophisticated user equipment will provide a best predictable positioning accuracy of 25 meters (2 drms), horizontally and 30 meters (2 sigma) vertically, velocity accuracy of 0.1 m/sec (1 sigma) in three dimensions and timing accuracy better than thirty nanoseconds (10^{-9} sec.).
- B. Repeatable accuracy will be the same as predictable accuracy.
- C. The best relative accuracy will be 13 meters (2 drms) horizontally and 15 meters (2 sigma) vertically.

3.7.3 Availability

NAVSTAR GPS will provide a 95% availability for the signal source needed to provide 25 meters (2 drms) horizontally and 30 meters (2 sigma) vertically predictable accuracy to users uniformly distributed on or near the earth. Availability of the NAVSTAR GPS signal for less accurate positioning will essentially be 100%.

3.7.4 Coverage

NAVSTAR GPS will provide worldwide, continuous coverage on the surface of the earth and up to 600 NM altitude.

3.7.5 Reliability

There are no operational reliability figures for the NAVSTAR GPS satellites. However, the planned satellite lifetime of 6 years corresponds to a single satellite reliability of about 90%. The constellation of 18 satellites will produce an overall reliability of 99+% for the satellite segment.

3.7.6 Fix Rate

The fix rate is essentially continuous. Actual time to produce a fix depends on user equipment capability and precise satellite geometry.

3.7.7 Fix Dimensions

NAVSTAR GPS provides three dimensional positioning and velocity fixes. In addition, it provides extremely accurate time information.

3.7.8 Capacity

The capacity of NAVSTAR GPS is unlimited.

3.7.9 Ambiguity Potential

NAVSTAR GPS has no ambiguity potential.

3.8 TRANSIT

TRANSIT is a space-based radio positioning navigational system consisting of five satellites in 600 NM polar orbits. The phasing of the satellites is deliberately staggered to minimize time-between-fixes for users. In addition, TRANSIT consists of four ground based monitors. The monitor stations track each satellite, while in view and provide the tracking information necessary to update satellite orbital parameters every 12 hours to one of the two tracking stations. Table III-3.6 describes the TRANSIT parameters.

3.8.1 Signal Characteristics

The satellites broadcast ephemeris information continuously on approximately 150 MHz and 400 MHz signals. One frequency is required to determine a position. However, by using the two frequencies, higher accuracy can be attained. A receiver measures successive doppler, or apparent frequency shifts of the signal, as the satellite approaches or passes the user. The receiver then calculates the geographic position of the user based on knowledge of the satellite position that is transmitted from the satellite every two minutes, and a knowledge of the Doppler shift of the satellite signal. Also, vessel course, speed, and time must be known accurately.

3.8.2 Accuracy

Predictable accuracy is 500m, repeatable accuracy is 50m, relative accuracy is 38m with a single satellite pass for a one-frequency user. A two-frequency user can compute his position with a predictable accuracy of 35m. Translocation (relative positioning) of land survey equipments can be accomplished to an accuracy of approximately one meter after reception and processing of multiple satellite passes.

3.8.3 Availability

Availability is 99+% when a TRANSIT satellite is in view.

3.8.4 Coverage

Coverage is worldwide but not continuous due to the relatively low altitude of the TRANSIT satellites.

3.8.5 Reliability

The reliability of the TRANSIT satellites is 99+%. This is due to the unusually long-lived satellites.

3.8.6 Fix Rate

Fix rate varies with latitude, theoretically from an average of 110 minutes at the equator to an average of 30 minutes at 80 degrees. Presently, due to non-uniform orbital precession, the TRANSIT satellites are no longer in evenly-spaced orbits. Due to this, a user can occasionally expect periods of between 6 and 11 hours when a fix is not available.

3.8.7 Fix Dimensions

TRANSIT provides two-dimensional navigational fixes.

3.8.8 Capacity

The capacity of TRANSIT is unlimited.

3.8.9 Ambiguity Potential

TRANSIT has no ambiguity potential.